

Vplyv geometrie na hodnotu efektívneho Poissonovho súčiniteľa auxetického metamateriálu

Semestrálna práca

2022/2023

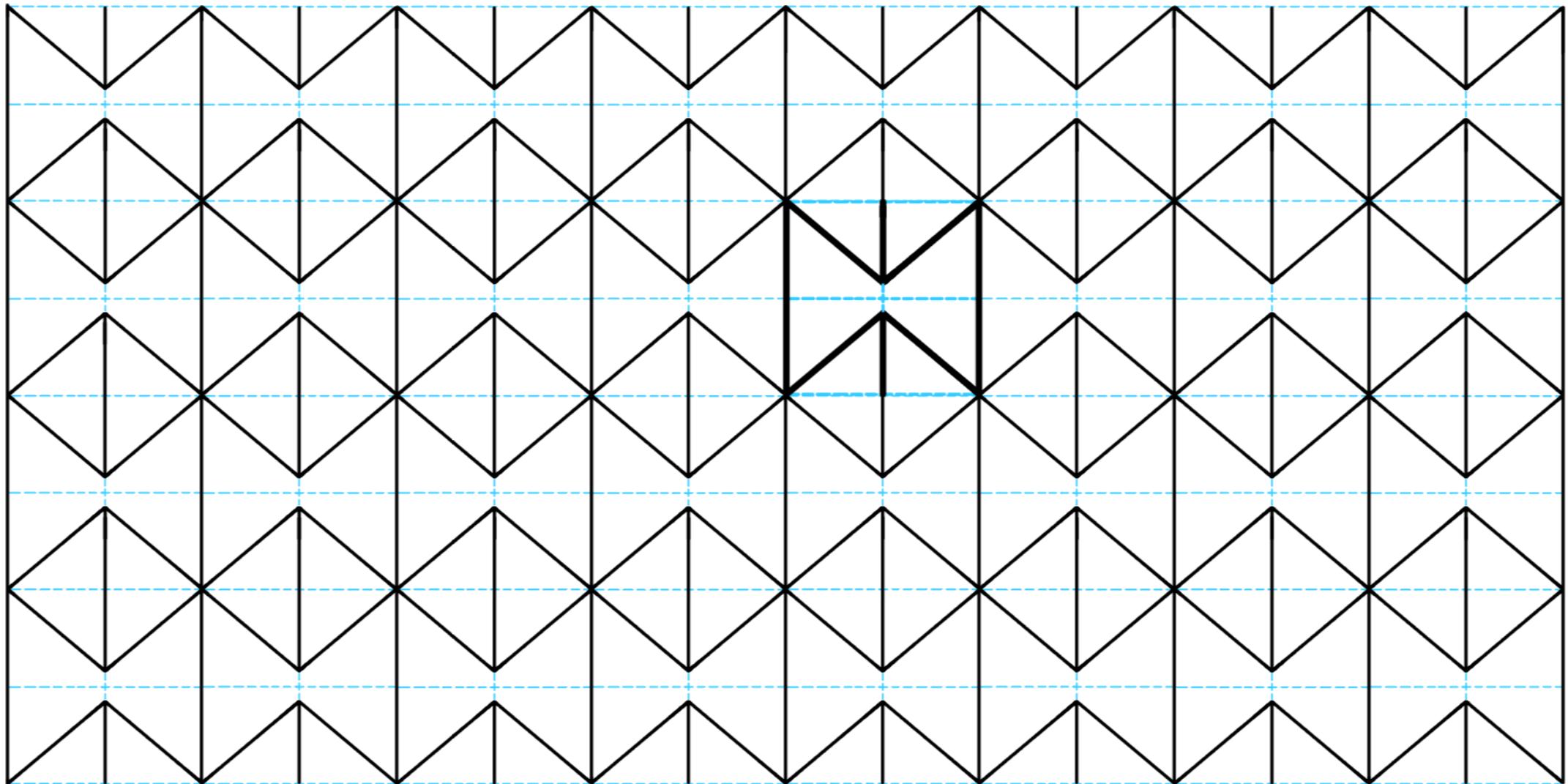
Pružnosť a pevnosť

Nataša Jošková

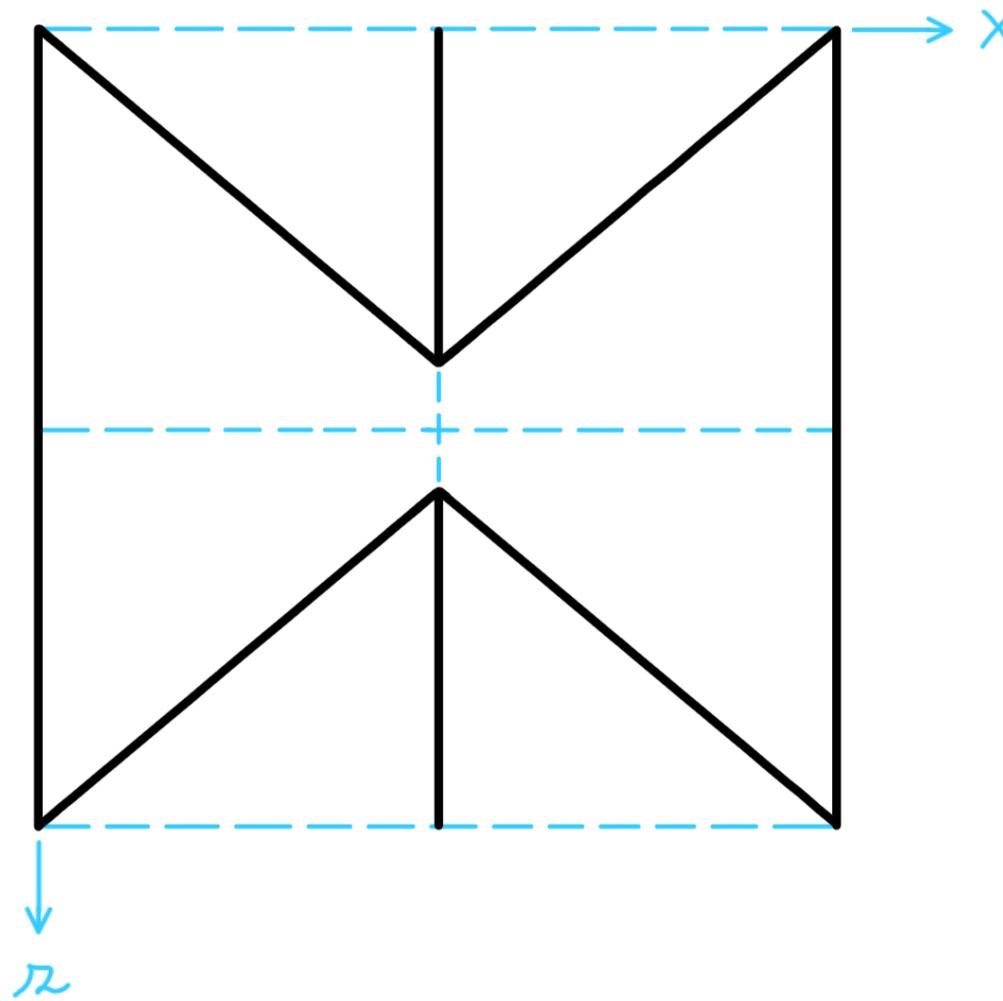
Katedra mechaniky

FSv ČVUT

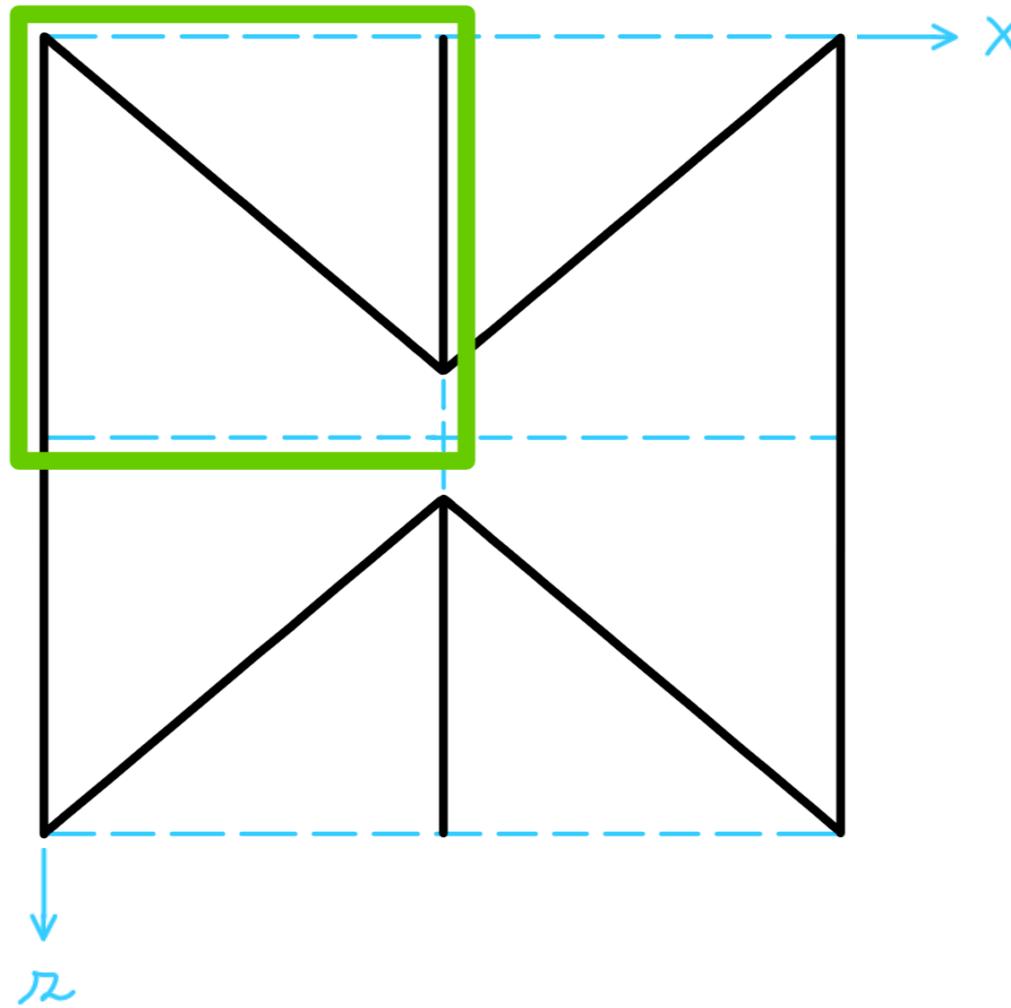
Auxetický metamateriál



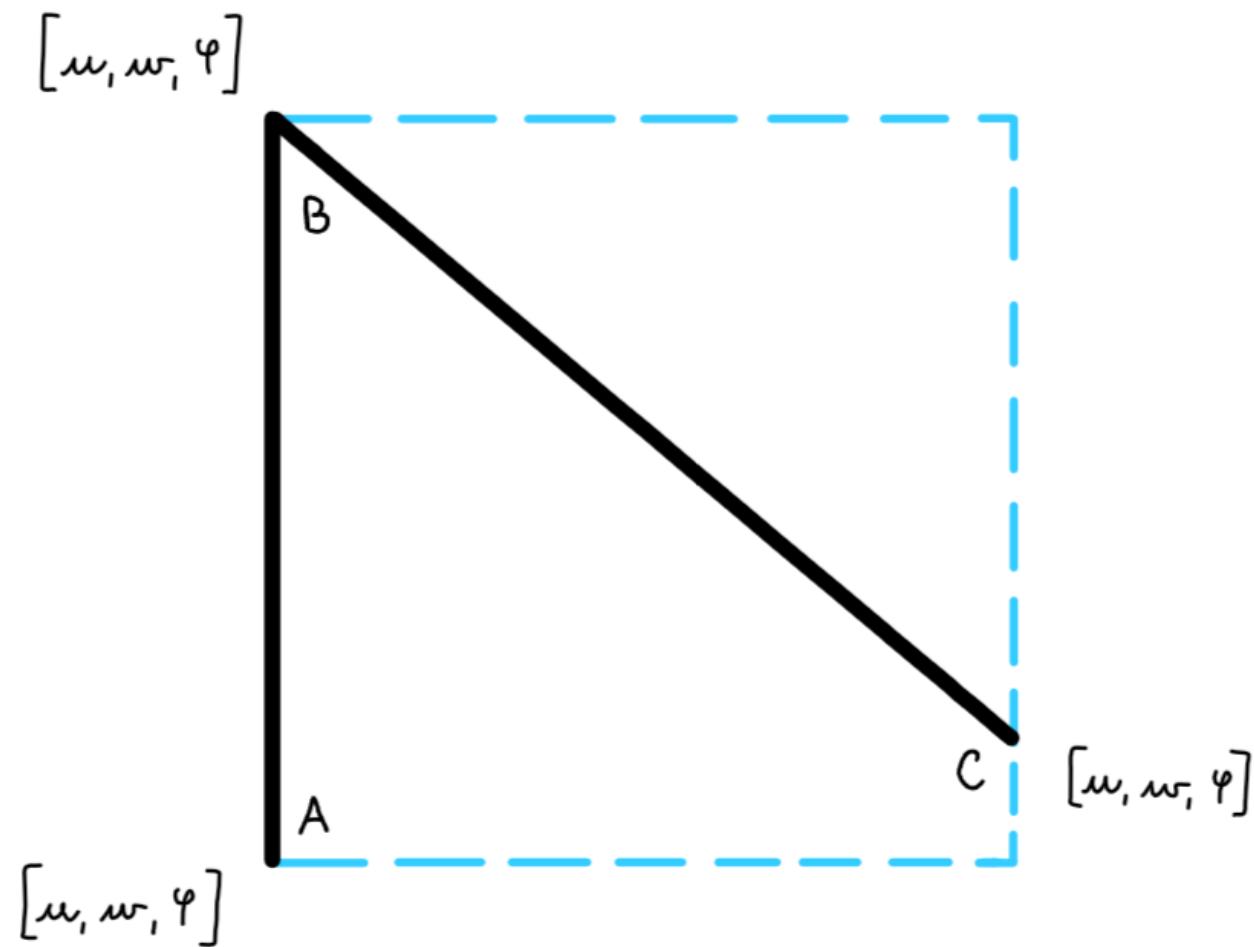
Zjednodušenie



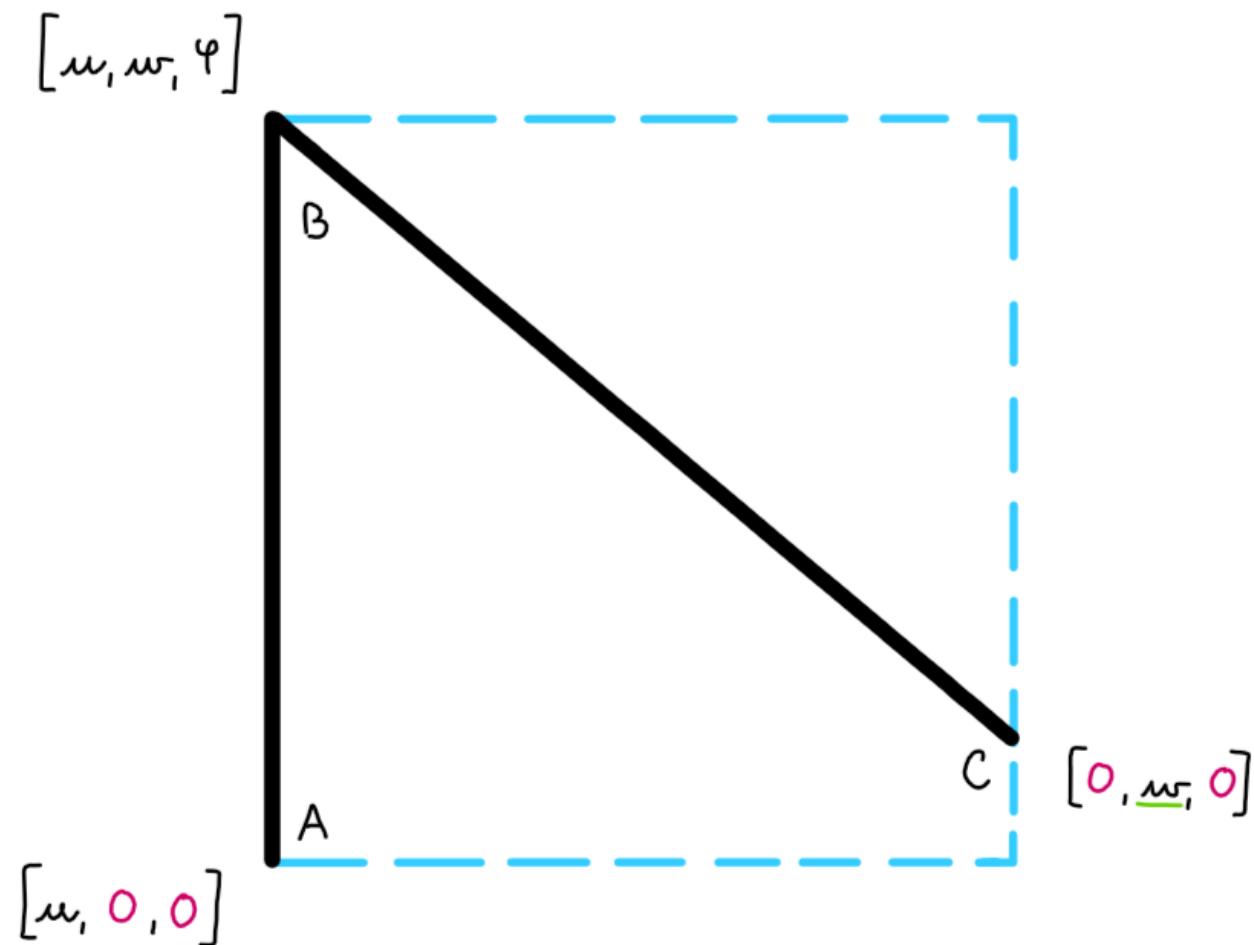
Zjednodušenie



Úvahy



Úvahy



Matica tuhosti prutu

$$\begin{Bmatrix} N_{ab} \\ V_{ab} \\ M_{ab} \\ N_{ba} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} k_{11} & k_{12} & k_{13} & k_{14} & k_{15} & k_{16} \\ k_{21} & k_{22} & k_{23} & k_{24} & k_{25} & k_{26} \\ k_{31} & k_{32} & k_{33} & k_{34} & k_{35} & k_{36} \\ k_{41} & k_{42} & k_{43} & k_{44} & k_{45} & k_{46} \\ k_{51} & k_{52} & k_{53} & k_{54} & k_{55} & k_{56} \\ k_{61} & k_{62} & k_{63} & k_{64} & k_{65} & k_{66} \end{bmatrix} \begin{Bmatrix} u_a \\ w_a \\ \varphi_a \\ u_b \\ w_b \\ \varphi_b \end{Bmatrix}$$

Vyjadrenie posunu u

$$\frac{d}{dx} \left[EA \frac{du}{dx}(x) \right] + \bar{f}_x(x) = 0$$

Normálová tuhost' prutu

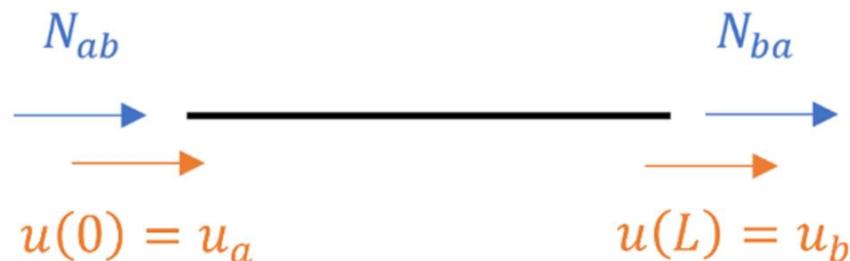
$$\varepsilon(x) = \frac{du}{dx}(x)$$

$$n_{ab} = \frac{EA}{L}$$

$$N = \frac{EA\Delta u}{L}$$

$$N_{ab} = n_{ab}(u_a - u_b)$$

$$N_{ba} = n_{ab}(u_b - u_a)$$



Matica tuhosti prutu

$$\begin{Bmatrix} N_{ab} \\ V_{ab} \\ M_{ab} \\ N_{ba} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} k_{11} & 0 & 0 & k_{14} & 0 & 0 \\ 0 & k_{22} & k_{23} & 0 & k_{25} & k_{26} \\ 0 & k_{32} & k_{33} & 0 & k_{35} & k_{36} \\ k_{41} & 0 & 0 & k_{44} & 0 & 0 \\ 0 & k_{52} & k_{53} & 0 & k_{55} & k_{56} \\ 0 & k_{62} & k_{63} & 0 & k_{65} & k_{66} \end{bmatrix} \begin{Bmatrix} u_a \\ w_a \\ \varphi_a \\ u_b \\ w_b \\ \varphi_b \end{Bmatrix}$$

$$\begin{Bmatrix} N_{ab} \\ V_{ab} \\ M_{ab} \\ N_{ba} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} n & 0 & 0 & -n & 0 & 0 \\ 0 & k_{22} & k_{23} & 0 & k_{25} & k_{26} \\ 0 & k_{32} & k_{33} & 0 & k_{35} & k_{36} \\ -n & 0 & 0 & n & 0 & 0 \\ 0 & k_{52} & k_{53} & 0 & k_{55} & k_{56} \\ 0 & k_{62} & k_{63} & 0 & k_{65} & k_{66} \end{bmatrix} \begin{Bmatrix} u_a \\ w_a \\ \varphi_a \\ u_b \\ w_b \\ \varphi_b \end{Bmatrix}$$

Matica tuhosti 4x4

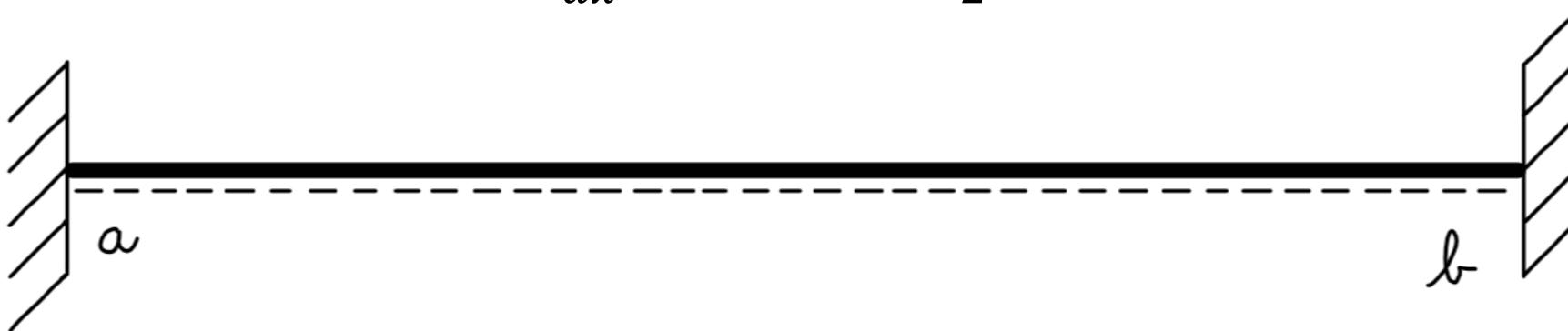
$$\begin{Bmatrix} V_{ab} \\ M_{ab} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} k_{22} & k_{23} & k_{25} & k_{26} \\ k_{32} & k_{33} & k_{35} & k_{36} \\ k_{52} & k_{53} & k_{55} & k_{56} \\ k_{62} & k_{63} & k_{65} & k_{66} \end{bmatrix} \begin{Bmatrix} w_a \\ \varphi_a \\ w_b \\ \varphi_b \end{Bmatrix}$$

Diferenciálna rovnica ohybovej čiary prutu

$$\frac{d^2}{dx^2} \left[EI_y \frac{d^2 w}{dx^2}(x) \right] = \bar{f}_z(x)$$

$$V = -EI_y \frac{d^3 w}{dx^3}(x) = -\bar{f}_z(x)x - c_1$$

$$M = -EI_y \frac{d^2 w}{dx^2}(x) = -\bar{f}_z(x) \frac{x^2}{2} - c_1 x - c_2$$



Matica tuhosti 4x4

$$\begin{Bmatrix} V_{ab} \\ M_{ab} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} k_{22} & k_{23} & k_{25} & k_{26} \\ k_{32} & k_{33} & k_{35} & k_{36} \\ k_{52} & k_{53} & k_{55} & k_{56} \\ k_{62} & k_{63} & k_{65} & k_{66} \end{bmatrix} \begin{Bmatrix} w_a \\ \varphi_a \\ w_b \\ \varphi_b \end{Bmatrix}$$

$$\begin{Bmatrix} V_{ab} \\ M_{ab} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} k_{22} & k_{23} & k_{25} & k_{26} \\ k_{32} & k_{33} & k_{35} & k_{36} \\ k_{52} & k_{53} & k_{55} & k_{56} \\ k_{62} & k_{63} & k_{65} & k_{66} \end{bmatrix} \begin{Bmatrix} 1 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

$$\begin{Bmatrix} V_{ab} \\ M_{ab} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} k_{22} & k_{23} & k_{25} & k_{26} \\ k_{32} & k_{33} & k_{35} & k_{36} \\ k_{52} & k_{53} & k_{55} & k_{56} \\ k_{62} & k_{63} & k_{65} & k_{66} \end{bmatrix} \begin{Bmatrix} 0 \\ 0 \\ 1 \\ 0 \end{Bmatrix}$$

$$\begin{Bmatrix} V_{ab} \\ M_{ab} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} k_{22} & k_{23} & k_{25} & k_{26} \\ k_{32} & k_{33} & k_{35} & k_{36} \\ k_{52} & k_{53} & k_{55} & k_{56} \\ k_{62} & k_{63} & k_{65} & k_{66} \end{bmatrix} \begin{Bmatrix} 0 \\ 1 \\ 0 \\ 0 \end{Bmatrix}$$

$$\begin{Bmatrix} V_{ab} \\ M_{ab} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} k_{22} & k_{23} & k_{25} & k_{26} \\ k_{32} & k_{33} & k_{35} & k_{36} \\ k_{52} & k_{53} & k_{55} & k_{56} \\ k_{62} & k_{63} & k_{65} & k_{66} \end{bmatrix} \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 1 \end{Bmatrix}$$

Matica tuhosti prutu

Ohybová tuhost' prutu $k_{ab} = \frac{2EI_y}{L}$

$$\begin{Bmatrix} V_{ab} \\ M_{ab} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} \frac{6k_{ab}}{L^2} & -\frac{3k_{ab}}{L} & -\frac{6k_{ab}}{L^2} & -\frac{3k_{ab}}{L} \\ -\frac{3k_{ab}}{L} & 2k_{ab} & \frac{3k_{ab}}{L} & k_{ab} \\ -\frac{6k_{ab}}{L^2} & \frac{3k_{ab}}{L} & \frac{6k_{ab}}{L^2} & \frac{3k_{ab}}{L} \\ -\frac{3k_{ab}}{L} & k_{ab} & \frac{3k_{ab}}{L} & 2k_{ab} \end{bmatrix} \begin{Bmatrix} w_a \\ \varphi_a \\ w_b \\ \varphi_b \end{Bmatrix}$$

$$\begin{Bmatrix} V_{ab} \\ M_{ab} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = k_{ab} \begin{bmatrix} \frac{6}{L^2} & -\frac{3}{L} & -\frac{6}{L^2} & -\frac{3}{L} \\ -\frac{3}{L} & 2 & \frac{3}{L} & 1 \\ -\frac{6}{L^2} & \frac{3}{L} & \frac{6}{L^2} & \frac{3}{L} \\ -\frac{3}{L} & 1 & \frac{3}{L} & 2 \end{bmatrix} \begin{Bmatrix} w_a \\ \varphi_a \\ w_b \\ \varphi_b \end{Bmatrix}$$

Vyjadrená matica tuhosti prutu

$$\begin{Bmatrix} N_{ab} \\ V_{ab} \\ M_{ab} \\ N_{ba} \\ V_{ba} \\ M_{ba} \end{Bmatrix} = \begin{bmatrix} n_{ab} & 0 & 0 & -n_{ab} & 0 & 0 \\ 0 & \frac{6k_{ab}}{L^2} & -\frac{3k_{ab}}{L} & 0 & -\frac{6k_{ab}}{L^2} & -\frac{3k_{ab}}{L} \\ 0 & -\frac{3k_{ab}}{L} & 2k_{ab} & 0 & \frac{3k_{ab}}{L} & k_{ab} \\ -n_{ab} & 0 & 0 & n_{ab} & 0 & 0 \\ 0 & -\frac{6k_{ab}}{L^2} & \frac{3k_{ab}}{L} & 0 & \frac{6k_{ab}}{L^2} & \frac{3k_{ab}}{L} \\ 0 & -\frac{3k_{ab}}{L} & k_{ab} & 0 & \frac{3k_{ab}}{L} & 2k_{ab} \end{bmatrix} \begin{Bmatrix} u_a \\ w_a \\ \varphi_a \\ u_b \\ w_b \\ \varphi_b \end{Bmatrix}$$

Transformácia súradníc

$$u_a^* = u_a \cos \alpha + w_a \sin \alpha$$

$$w_a^* = -u_a \sin \alpha + w_a \cos \alpha$$

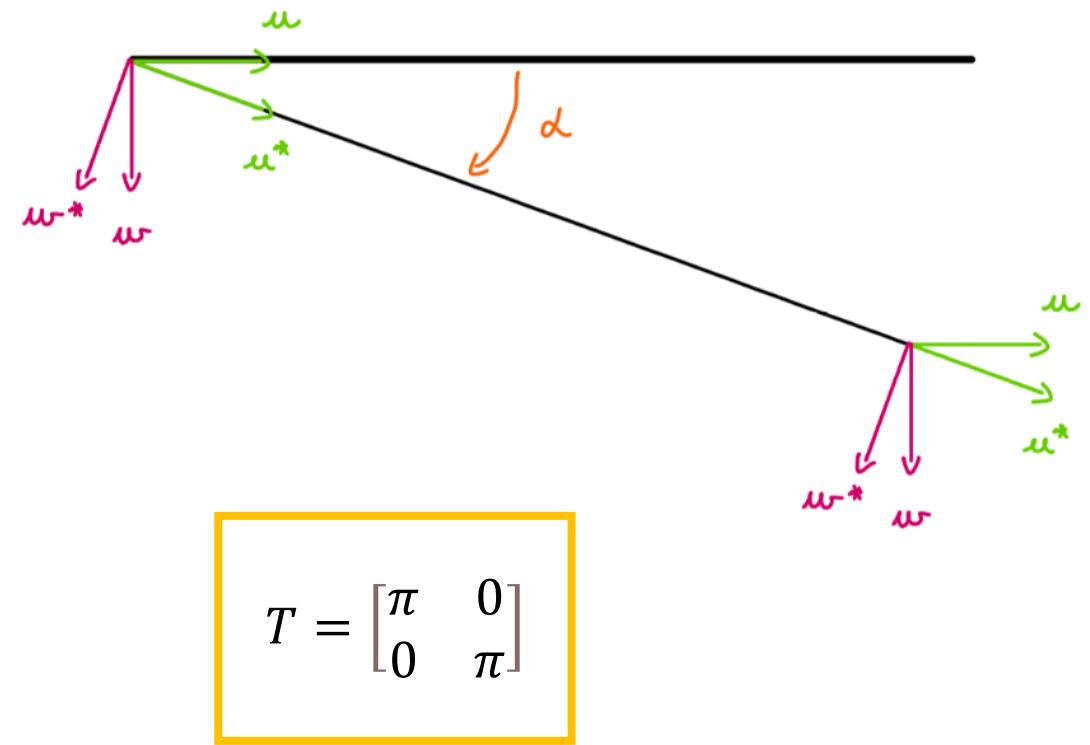
$$\varphi_a^* = \varphi_a$$

$$u_b^* = u_b \cos \alpha + w_b \sin \alpha$$

$$w_b^* = -u_b \sin \alpha + w_b \cos \alpha$$

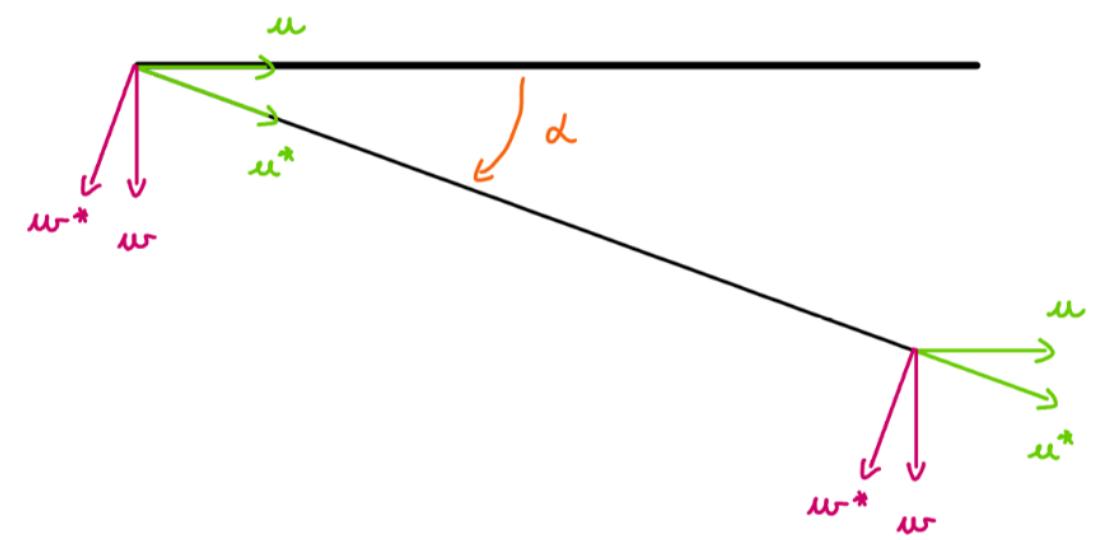
$$\varphi_b^* = \varphi_b$$

$$\begin{bmatrix} u^* \\ w^* \\ \varphi^* \end{bmatrix} = \begin{bmatrix} \cos \alpha & \sin \alpha & 0 \\ -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} u \\ w \\ \varphi \end{bmatrix} = \pi \begin{bmatrix} u \\ w \\ \varphi \end{bmatrix}$$



Transformácia súradníc

$$T = \begin{bmatrix} \cos \alpha & \sin \alpha & 0 & 0 & 0 & 0 \\ -\sin \alpha & \cos \alpha & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & \cos \alpha & \sin \alpha & 0 \\ 0 & 0 & 0 & -\sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

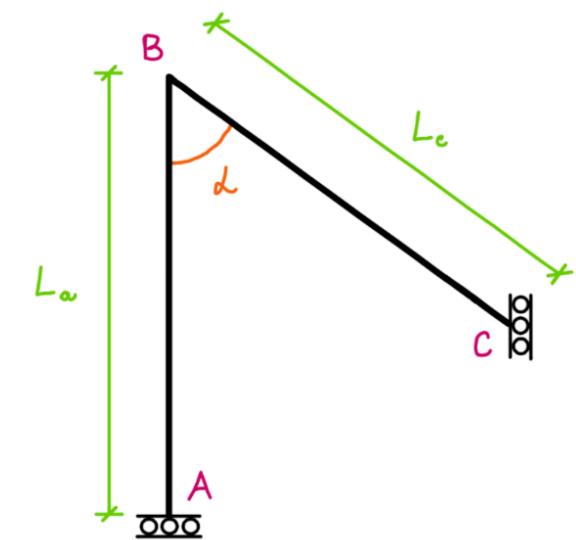


$$T^T = \begin{bmatrix} \cos \alpha & -\sin \alpha & 0 & 0 & 0 & 0 \\ \sin \alpha & \cos \alpha & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 & 0 & 0 \\ 0 & 0 & 0 & \cos \alpha & -\sin \alpha & 0 \\ 0 & 0 & 0 & \sin \alpha & \cos \alpha & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix}$$

$$K^g = T^T K^l T$$

Matica tuhosti v globálnom SS

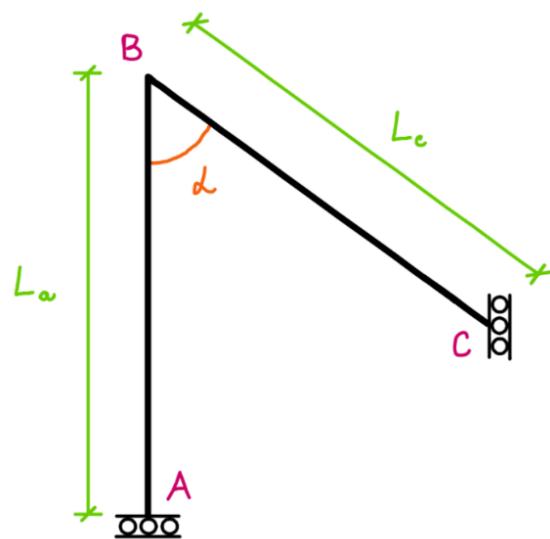
$$\begin{bmatrix} N_a^* \\ V_a^* \\ M_a^* \\ N_b^* \\ V_b^* \\ M_b^* \end{bmatrix} = \begin{bmatrix} n_{ab}\cos^2\alpha + \frac{6k_{ab}}{L^2}\sin^2\alpha & \left(n_{ab} - \frac{6k_{ab}}{L^2}\right)\sin\alpha\cos\alpha & \frac{3k_{ab}}{L}\sin\alpha & -n_{ab}\cos^2\alpha - \frac{6k_{ab}}{L^2}\sin^2\alpha & \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha & \frac{3k_{ab}}{L}\sin\alpha \\ \left(n_{ab} - \frac{6k_{ab}}{L^2}\right)\sin\alpha\cos\alpha & n_{ab}\sin^2\alpha + \frac{6k_{ab}}{L^2}\cos^2\alpha & -\frac{3k_{ab}}{L}\cos\alpha & \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha & -n_{ab}\sin^2\alpha - \frac{6k_{ab}}{L^2}\cos^2\alpha & -\frac{3k_{ab}}{L}\cos\alpha \\ \frac{3k_{ab}}{L}\sin\alpha & -\frac{3k_{ab}}{L}\cos\alpha & 2k_{ab} & -\frac{3k_{ab}}{L}\sin\alpha & \frac{3k_{ab}}{L}\cos\alpha & k_{ab} \\ -n_{ab}\cos^2\alpha - \frac{6k_{ab}}{L^2}\sin^2\alpha & \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha & -\frac{3k_{ab}}{L}\sin\alpha & n_{ab}\cos^2\alpha + \frac{6k_{ab}}{L^2}\sin^2\alpha & \left(n_{ab} - \frac{6k_{ab}}{L^2}\right)\sin\alpha\cos\alpha & -\frac{3k_{ab}}{L}\sin\alpha \\ \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha & -n_{ab}\sin^2\alpha - \frac{6k_{ab}}{L^2}\cos^2\alpha & \frac{3k_{ab}}{L}\cos\alpha & \left(n_{ab} - \frac{6k_{ab}}{L^2}\right)\sin\alpha\cos\alpha & n_{ab}\sin^2\alpha + \frac{6k_{ab}}{L^2}\cos^2\alpha & \frac{3k_{ab}}{L}\cos\alpha \\ \frac{3k_{ab}}{L}\sin\alpha & -\frac{3k_{ab}}{L}\cos\alpha & k_{ab} & -\frac{3k_{ab}}{L}\sin\alpha & \frac{3k_{ab}}{L}\cos\alpha & 2k_{ab} \end{bmatrix} \begin{bmatrix} u_a \\ w_a \\ \varphi_a \\ u_b \\ w_b \\ \varphi_b \end{bmatrix}$$



Matica tuhosti pre sústavu 2 prutov

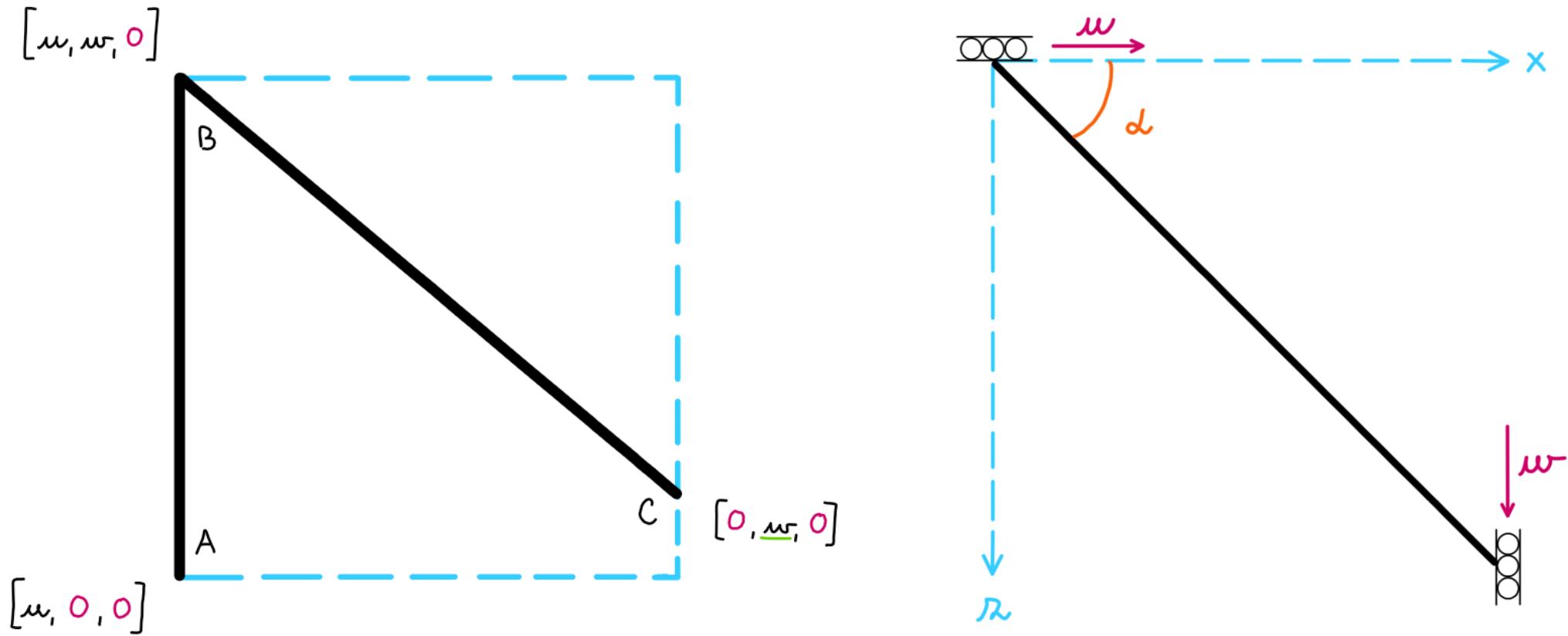
$$\begin{pmatrix}
 X_{ab} \\
 Z_{ab} \\
 M_{ab} \\
 X_b \\
 Z_b \\
 M_b \\
 X_{cb} \\
 Z_{cb} \\
 M_{cb}
 \end{pmatrix} =
 \begin{pmatrix}
 0 & n_{ab} & 0 & 0 & -n_{ab} & 0 & 0 & 0 & 0 \\
 \frac{6k_{ab}}{L_a^2} & 0 & -\frac{3k_{ab}}{L_a} & -\frac{6k_{ab}}{L_a^2} & 0 & -\frac{3k_{ab}}{L_a} & 0 & 0 & 0 \\
 -\frac{3k_{ab}}{L_a} & 0 & 2k_{ab} & \frac{3k_{ab}}{L_a} & 0 & k_{ab} & 0 & 0 & 0 \\
 0 & -n_{ab} & 0 & n_{bc}\cos^2\alpha + \frac{6k_{bc}}{L_c^2}\sin^2\alpha & \left(n_{bc} - \frac{6k_{bc}}{L_c^2}\right)\sin\alpha\cos\alpha & \frac{3k_{bc}}{L_c}\sin\alpha & -n_{bc}\cos^2\alpha - \frac{6k_{bc}}{L_c^2}\sin^2\alpha & \left(\frac{6k_{bc}}{L_c^2} - n_{bc}\right)\sin\alpha\cos\alpha & \frac{3k_{bc}}{L_c}\sin\alpha \\
 -\frac{6k_{ab}}{L_a^2} & 0 & \frac{3k_{ab}}{L_a} & \frac{6k_{ab}}{L_a^2} + \left(n_{bc} - \frac{6k_{bc}}{L_c^2}\right)\sin\alpha\cos\alpha & n_{bc}\sin^2\alpha + \frac{6k_{bc}}{L_c^2}\cos^2\alpha & \frac{3k_{ab}}{L_a} - \frac{3k_{bc}}{L_c}\cos\alpha & \left(\frac{6k_{bc}}{L_c^2} - n_{bc}\right)\sin\alpha\cos\alpha & -n_{bc}\sin^2\alpha - \frac{6k_{bc}}{L_c^2}\cos^2\alpha & -\frac{3k_{bc}}{L_c}\cos\alpha \\
 -\frac{3k_{ab}}{L_a} & 0 & k_{ab} & \frac{3k_{ab}}{L_a} + \frac{3k_{bc}}{L_c}\sin\alpha & -\frac{3k_{bc}}{L_c}\cos\alpha & 2k_{ab} + 2k_{bc} & -\frac{3k_{bc}}{L_c}\sin\alpha & \frac{3k_{bc}}{L_c}\cos\alpha & k_{bc} \\
 0 & 0 & 0 & -n_{bc}\cos^2\alpha - \frac{6k_{bc}}{L_c^2}\sin^2\alpha & \left(\frac{6k_{bc}}{L_c^2} - n_{bc}\right)\sin\alpha\cos\alpha & -\frac{3k_{bc}}{L_c}\sin\alpha & n_{bc}\cos^2\alpha + \frac{6k_{bc}}{L_c^2}\sin^2\alpha & \left(n_{bc} - \frac{6k_{bc}}{L_c^2}\right)\sin\alpha\cos\alpha & -\frac{3k_{bc}}{L_c}\sin\alpha \\
 0 & 0 & 0 & \left(\frac{6k_{bc}}{L_c^2} - n_{bc}\right)\sin\alpha\cos\alpha & -n_{bc}\sin^2\alpha - \frac{6k_{bc}}{L_c^2}\cos^2\alpha & \frac{3k_{bc}}{L_c}\cos\alpha & \left(n_{bc} - \frac{6k_{bc}}{L_c^2}\right)\sin\alpha\cos\alpha & n_{bc}\sin^2\alpha + \frac{6k_{bc}}{L_c^2}\cos^2\alpha & \frac{3k_{bc}}{L_c}\cos\alpha \\
 0 & 0 & 0 & \frac{3k_{bc}}{L_c}\sin\alpha & -\frac{3k_{bc}}{L_c}\cos\alpha & k_{bc} & -\frac{3k_{bc}}{L_c}\sin\alpha & \frac{3k_{bc}}{L_c}\cos\alpha & 2k_{bc}
 \end{pmatrix} \begin{pmatrix}
 u_a \\
 w_a \\
 \varphi_a \\
 u_b \\
 w_b \\
 \varphi_b \\
 u_c \\
 w_c \\
 \varphi_c
 \end{pmatrix}$$

Matica tuhosti pre sústavu 2 prutov



$$\begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix} = \begin{bmatrix} 0 & 0 & -\frac{EA}{L_a} & 0 \\ 0 & \frac{EA}{L_c} \cos^2 \alpha + \frac{12EI_y}{L_c^3} \sin^2 \alpha & \left(\frac{EA}{L_c} - \frac{12EI_y}{L_c^3} \right) \sin \alpha \cos \alpha & \frac{6EI_y}{L_c^2} \sin \alpha \\ -\frac{12EI_y}{L_a^3} & \frac{12EI_y}{L_a^3} + \left(\frac{EA}{L_c} - \frac{12EI_y}{L_c^3} \right) \sin \alpha \cos \alpha & \frac{EA}{L_c} \sin^2 \alpha + \frac{12EI_y}{L_c^3} \cos^2 \alpha & \frac{6EI_y}{L_a^2} - \frac{6EI_y}{L_c^2} \cos \alpha \\ -\frac{6EI_y}{L_a^2} & \frac{6EI_y}{L_a^2} + \frac{6EI_y}{L_c^2} \sin \alpha & -\frac{6EI_y}{L_c^2} \cos \alpha & \frac{4EI_y}{L_a} + \frac{4EI_y}{L_c} \\ 0 & \left(\frac{12EI_y}{L_c^3} - \frac{EA}{L_c} \right) \sin \alpha \cos \alpha & -\frac{EA}{L_c} \sin^2 \alpha - \frac{12EI_y}{L_c^3} \cos^2 \alpha & \frac{6EI_y}{L_c^2} \cos \alpha \\ \end{bmatrix} \begin{Bmatrix} u_a \\ u_b \\ w_b \\ \varphi_b \\ w_c \end{Bmatrix}$$

Model auxetického metamateriálu s jedným prutom



Matica tuhosti modelu s jedným prutom

$$\begin{pmatrix} X_b^* \\ Z_b^* \\ M_b^* \\ X_c^* \\ Z_c^* \\ M_c^* \end{pmatrix} = \begin{pmatrix} n_{ab}\cos^2\alpha + \frac{6k_{ab}}{L^2}\sin^2\alpha & \left(n_{ab} - \frac{6k_{ab}}{L^2}\right)\sin\alpha\cos\alpha & \frac{3k_{ab}}{L}\sin\alpha & -n_{ab}\cos^2\alpha - \frac{6k_{ab}}{L^2}\sin^2\alpha & \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha & \frac{3k_{ab}}{L}\sin\alpha \\ \left(n_{ab} - \frac{6k_{ab}}{L^2}\right)\sin\alpha\cos\alpha & n_{ab}\sin^2\alpha + \frac{6k_{ab}}{L^2}\cos^2\alpha & -\frac{3k_{ab}}{L}\cos\alpha & \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha & -n_{ab}\sin^2\alpha - \frac{6k_{ab}}{L^2}\cos^2\alpha & -\frac{3k_{ab}}{L}\cos\alpha \\ \frac{3k_{ab}}{L}\sin\alpha & -\frac{3k_{ab}}{L}\cos\alpha & 2k_{ab} & -\frac{3k_{ab}}{L}\sin\alpha & \frac{3k_{ab}}{L}\cos\alpha & k_{ab} \\ -n_{ab}\cos^2\alpha - \frac{6k_{ab}}{L^2}\sin^2\alpha & \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha & -\frac{3k_{ab}}{L}\sin\alpha & n_{ab}\cos^2\alpha + \frac{6k_{ab}}{L^2}\sin^2\alpha & \left(n_{ab} - \frac{6k_{ab}}{L^2}\right)\sin\alpha\cos\alpha & -\frac{3k_{ab}}{L}\sin\alpha \\ \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha & -n_{ab}\sin^2\alpha - \frac{6k_{ab}}{L^2}\cos^2\alpha & \frac{3k_{ab}}{L}\cos\alpha & \left(n_{ab} - \frac{6k_{ab}}{L^2}\right)\sin\alpha\cos\alpha & n_{ab}\sin^2\alpha + \frac{6k_{ab}}{L^2}\cos^2\alpha & \frac{3k_{ab}}{L}\cos\alpha \\ \frac{3k_{ab}}{L}\sin\alpha & -\frac{3k_{ab}}{L}\cos\alpha & k_{ab} & -\frac{3k_{ab}}{L}\sin\alpha & \frac{3k_{ab}}{L}\cos\alpha & 2k_{ab} \end{pmatrix} \begin{pmatrix} u_b \\ w_b \\ \varphi_b \\ u_c \\ w_c \\ \varphi_c \end{pmatrix}$$

$$\begin{pmatrix} 0 \\ R_c \end{pmatrix} = \begin{pmatrix} n_{ab}\cos^2\alpha + \frac{6k_{ab}}{L^2}\sin^2\alpha & \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha \\ \left(\frac{6k_{ab}}{L^2} - n_{ab}\right)\sin\alpha\cos\alpha & n_{ab}\sin^2\alpha + \frac{6k_{ab}}{L^2}\cos^2\alpha \end{pmatrix} \begin{pmatrix} u_b \\ w_c \end{pmatrix}$$

Vzťah medzi posunmi u_a a w_b

$$0 = \frac{L^2 E A \cos^2 \alpha + 12 E I_y \sin^2 \alpha}{L^3} u_b + \left(\frac{12 E I_y - L^2 E A}{L^3} \right) \sin \alpha \cos \alpha w_c$$

$$u_b = - \frac{(12 I_y - L^2 A) \sin \alpha \cos \alpha}{L^2 A \cos^2 \alpha + 12 I_y \sin^2 \alpha} w_c$$

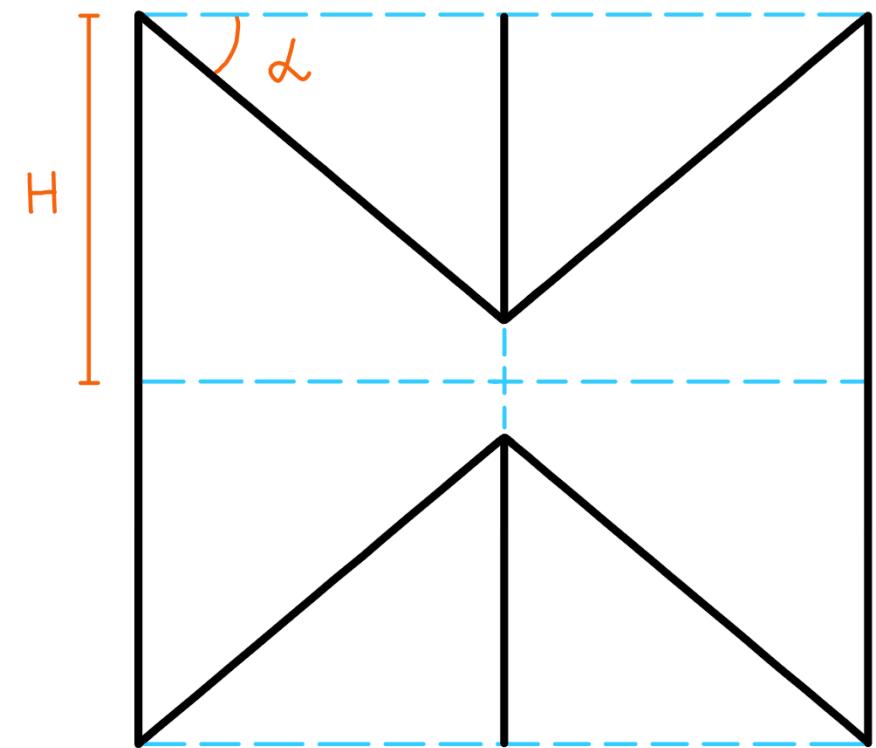
Vzťah medzi posunmi u_a a w_b

polomer zotrvačnosti

$$i^2 = \frac{I_y}{A}$$

$$L = \frac{H}{\cos \alpha}$$

$$u_b = -\frac{\left(12i^2 - \frac{H^2}{\cos^2 \alpha}\right) \sin \alpha \cos \alpha}{H^2 + 12i^2 \sin^2 \alpha} w_c$$

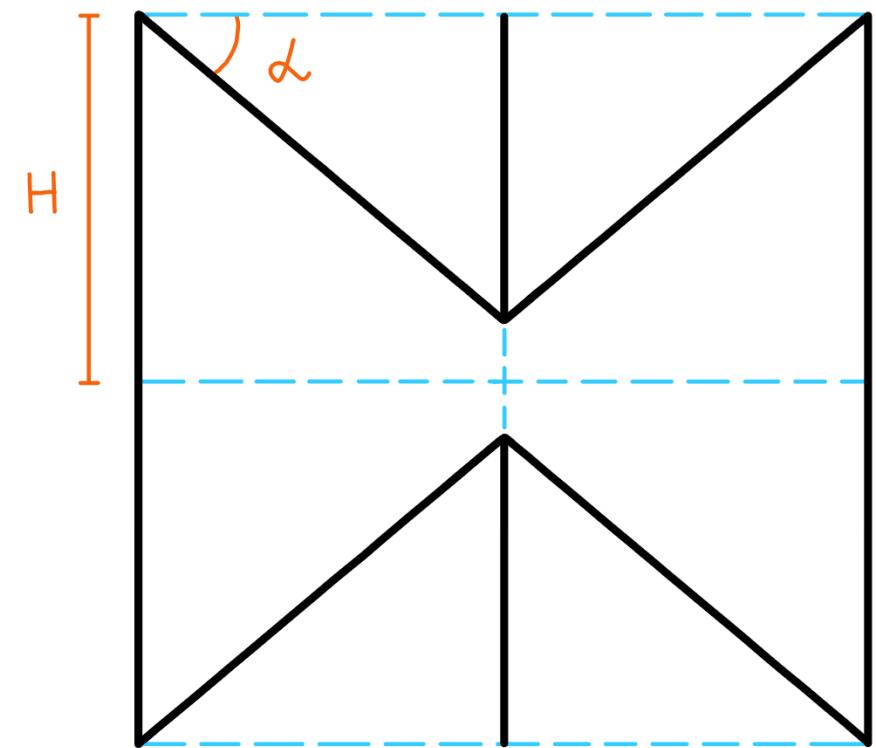


Vzťah medzi posunmi u_a a w_b

parameter λ

$$\lambda = \frac{i}{H}$$

$$u_b = -\frac{\left(12\lambda^2 - \frac{1}{\cos^2 \alpha}\right) \sin \alpha \cos \alpha}{1 + 12\lambda^2 \sin^2 \alpha} w_c$$



Poissonovo číslo ν

$$\nu = -\frac{\frac{u_b}{L}}{\frac{w_c}{L}}$$

$$\nu = -\frac{u_b}{w_c}$$

$$\nu = -\frac{\varepsilon_x}{\varepsilon_z}$$

Pomerná deformácia

$$\varepsilon_x \approx \frac{u_b}{L}$$

$$\varepsilon_z \approx \frac{w_c}{L}$$

$$\nu = \frac{\left(12\lambda^2 - \frac{1}{\cos^2 \alpha}\right) \sin \alpha \cos \alpha}{1 + 12\lambda^2 \sin^2 \alpha}$$

Poissonovo číslo ν

$$\lambda \ll 1$$

$$\nu \approx -\frac{1}{\cos^2 \alpha} \sin \alpha \cos \alpha$$

$$\nu \approx -\frac{\sin \alpha}{\cos \alpha}$$

$$\nu \approx -\tan \alpha$$

Vplyv geometrie auxetického metamateriálu

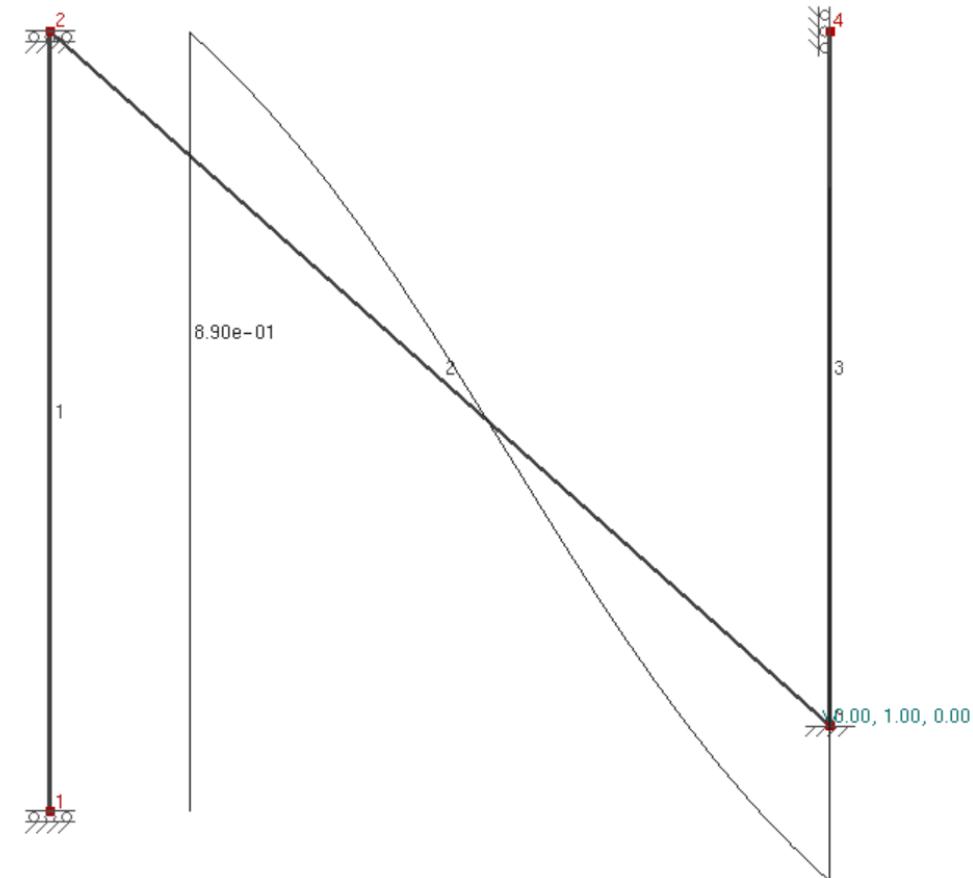
$G = \infty$

$w = 1 \text{ m}$

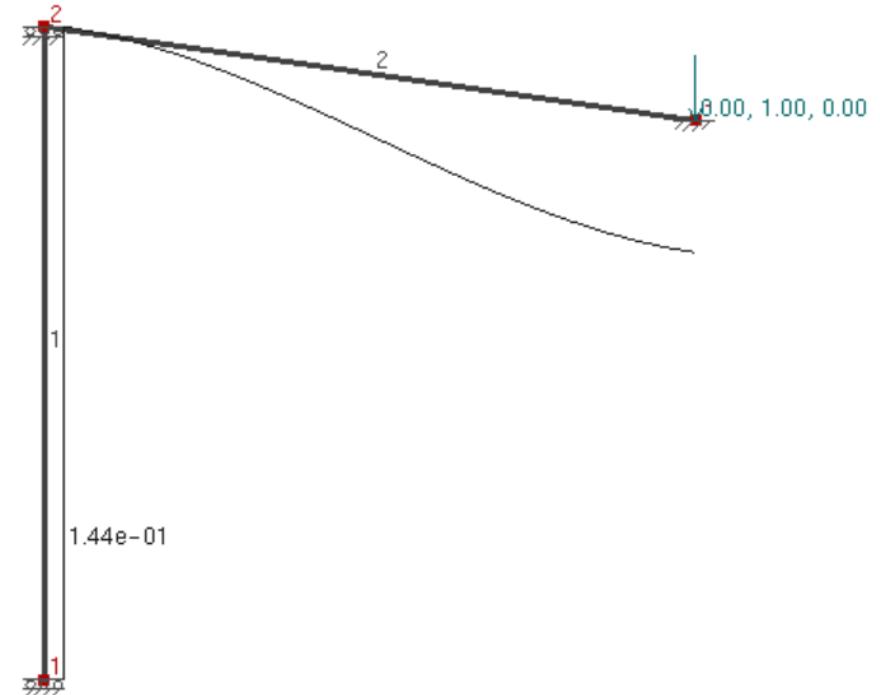
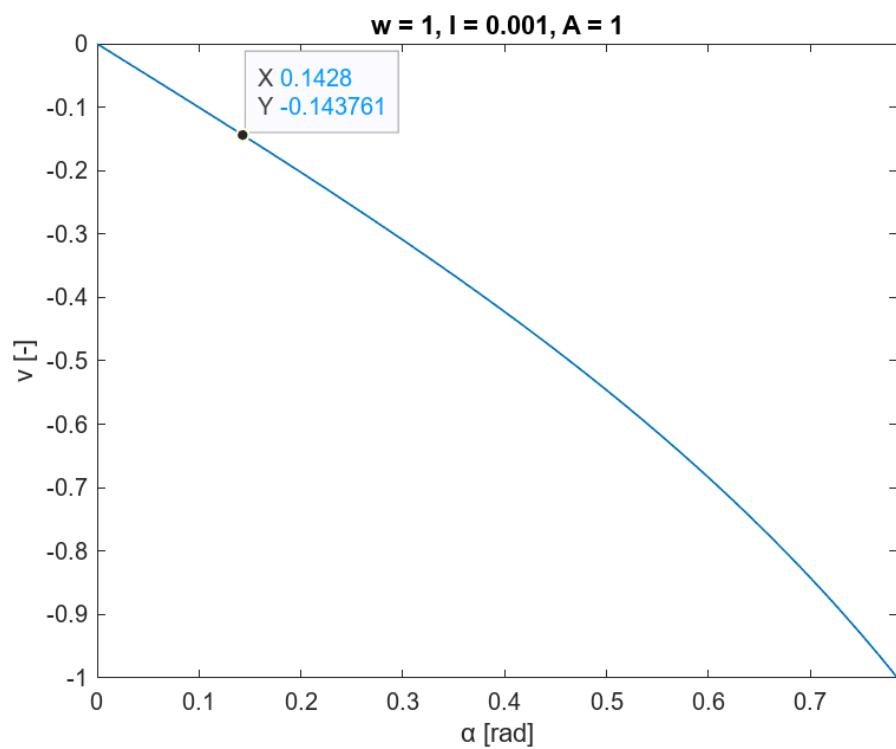
$H = 10 \text{ m}$

$I_y = 0.001 \text{ m}^4$

$A = 1 \text{ m}^2$

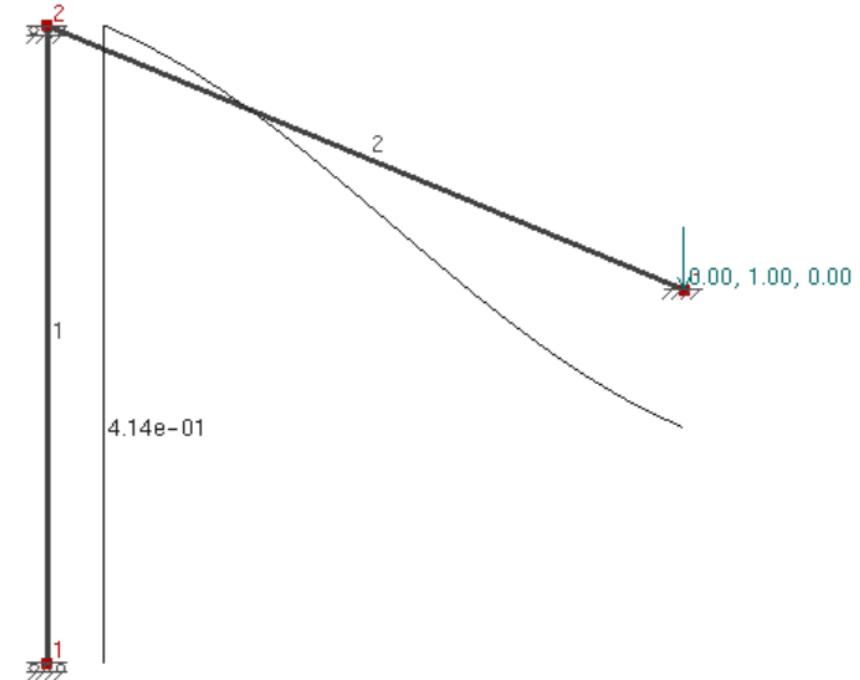
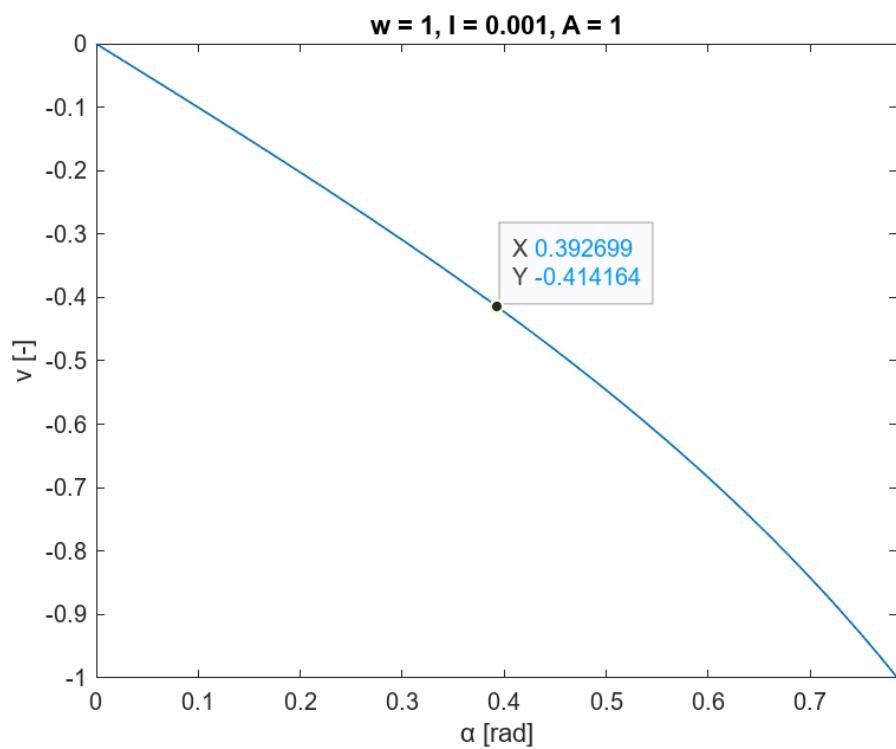


$$\alpha = 8.1818^\circ$$



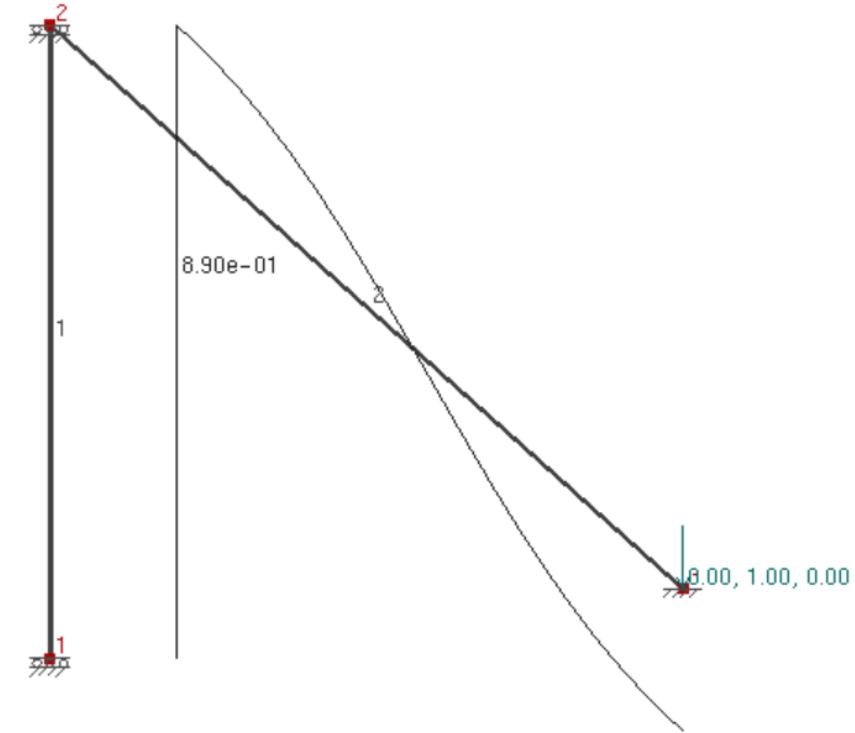
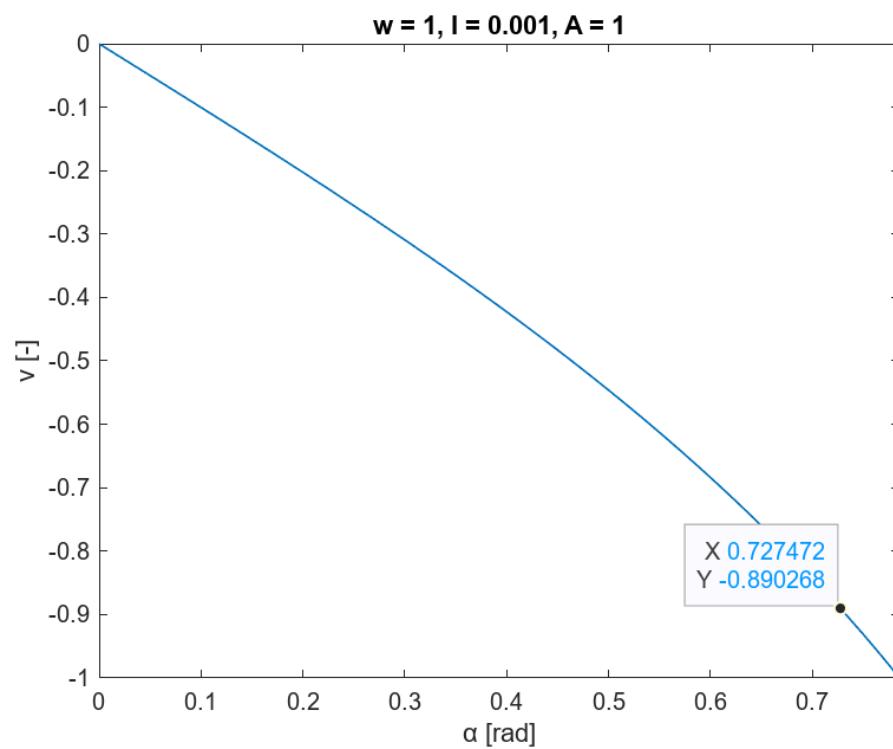
Uzel	x [~m]	y [~m]	z [~m]	u [~m]	w [~m]	phi [~rad]
1	0	0	10	0.14376275	0	0
2	0	0	0	0.14376275	0	0
3	10	0	1.4378	0	1	0

$$\alpha = 22.5^\circ$$



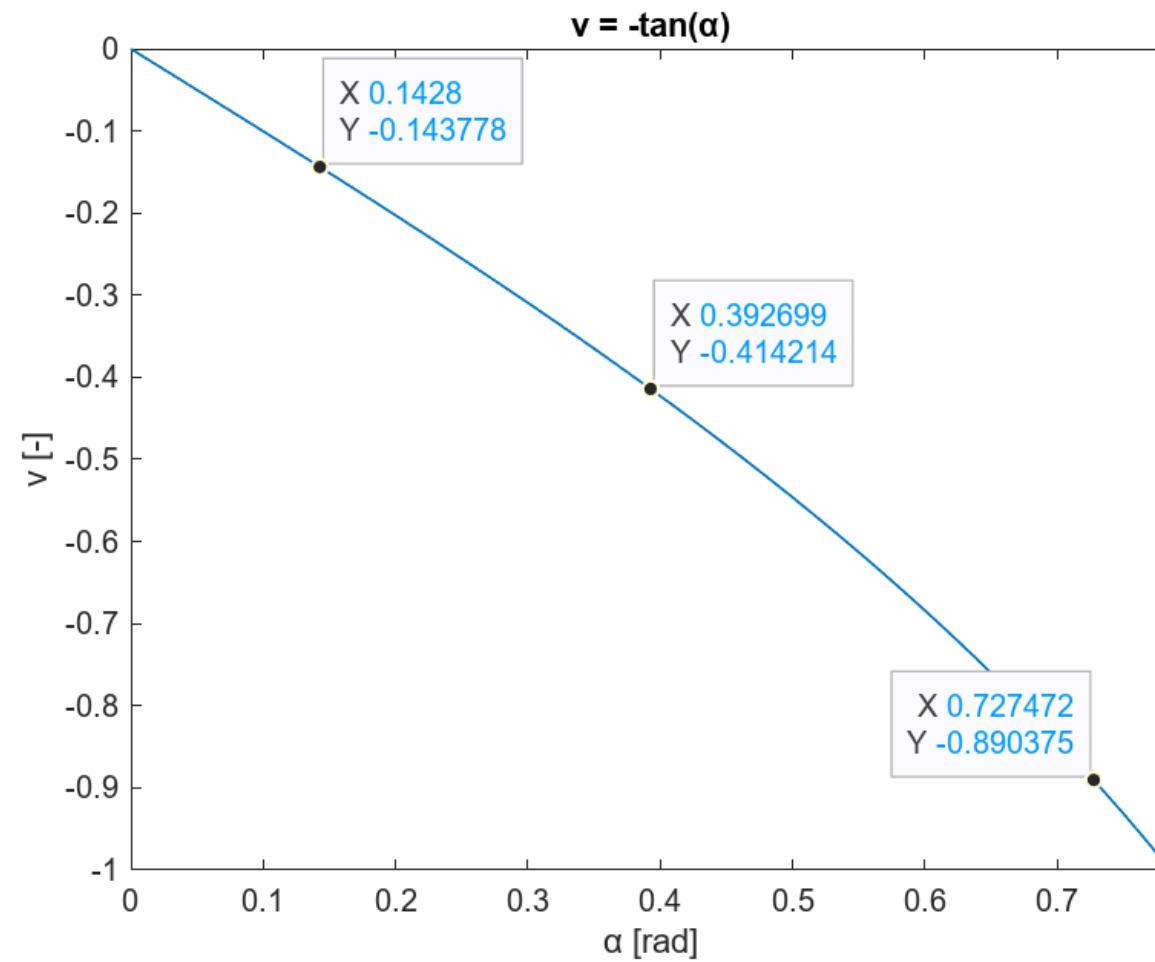
Uzel	x [~m]	y [~m]	z [~m]	u [~m]	w [~m]	phi [~rad]
1	0	0	10	0.4141603	0	0
2	0	0	0	0.4141603	0	0
3	10	0	4.1421	0	1	0

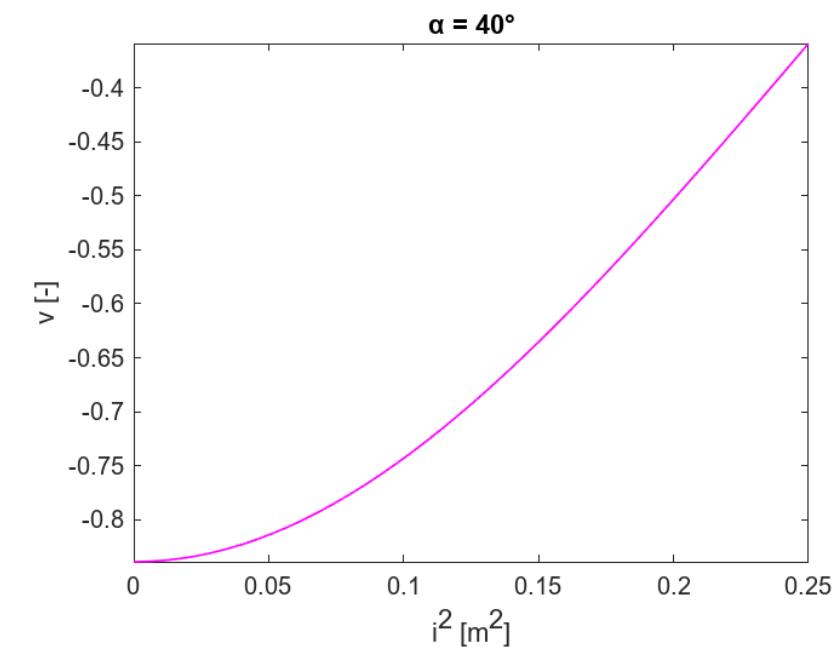
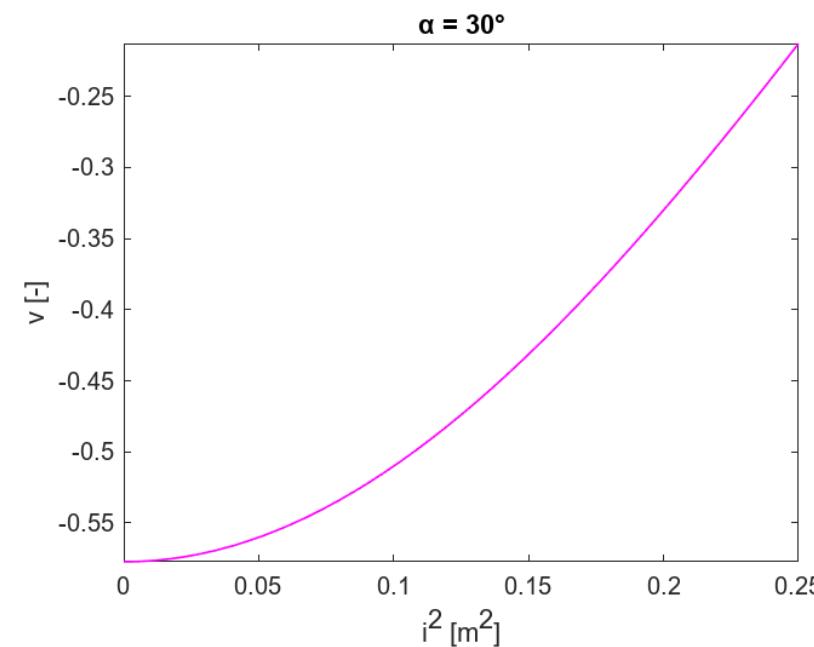
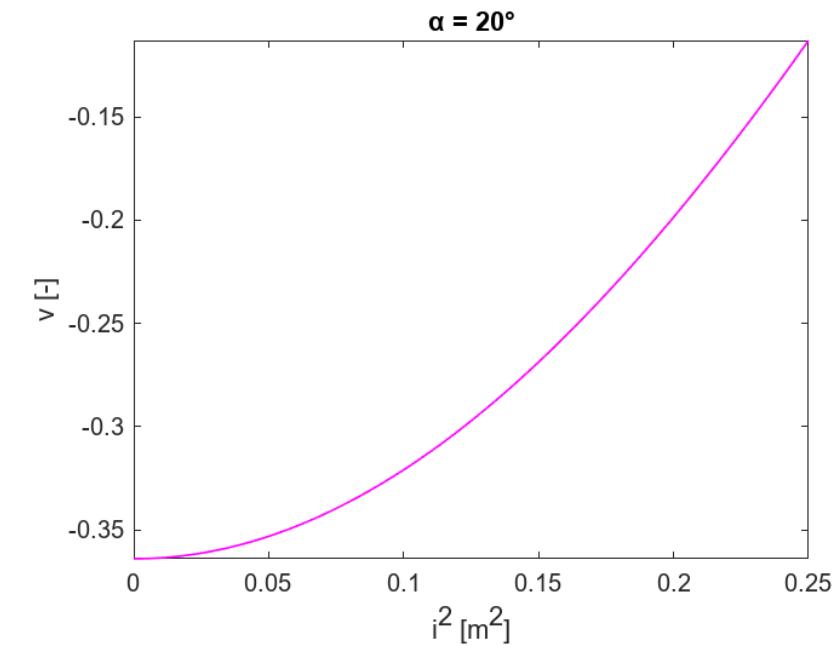
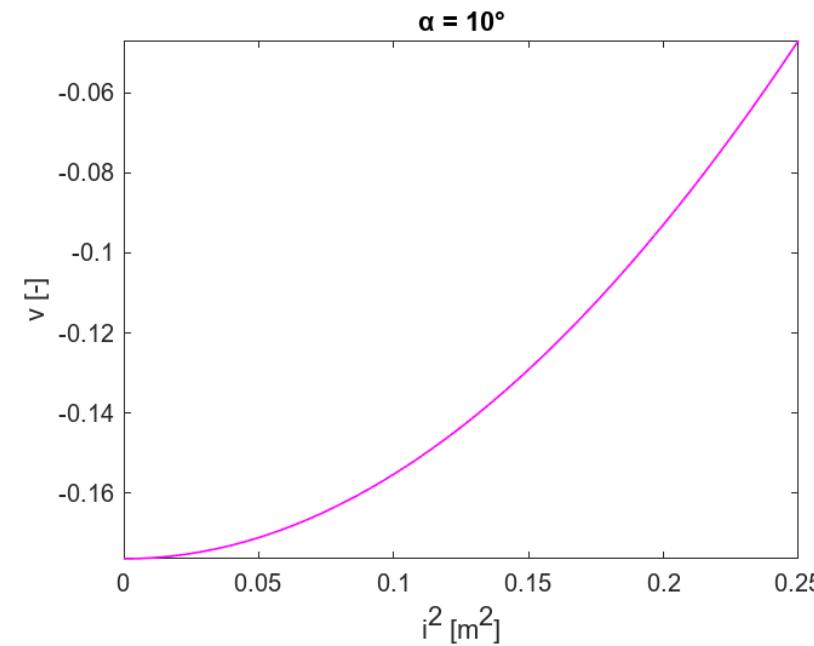
$$\alpha = 41.6811^\circ$$

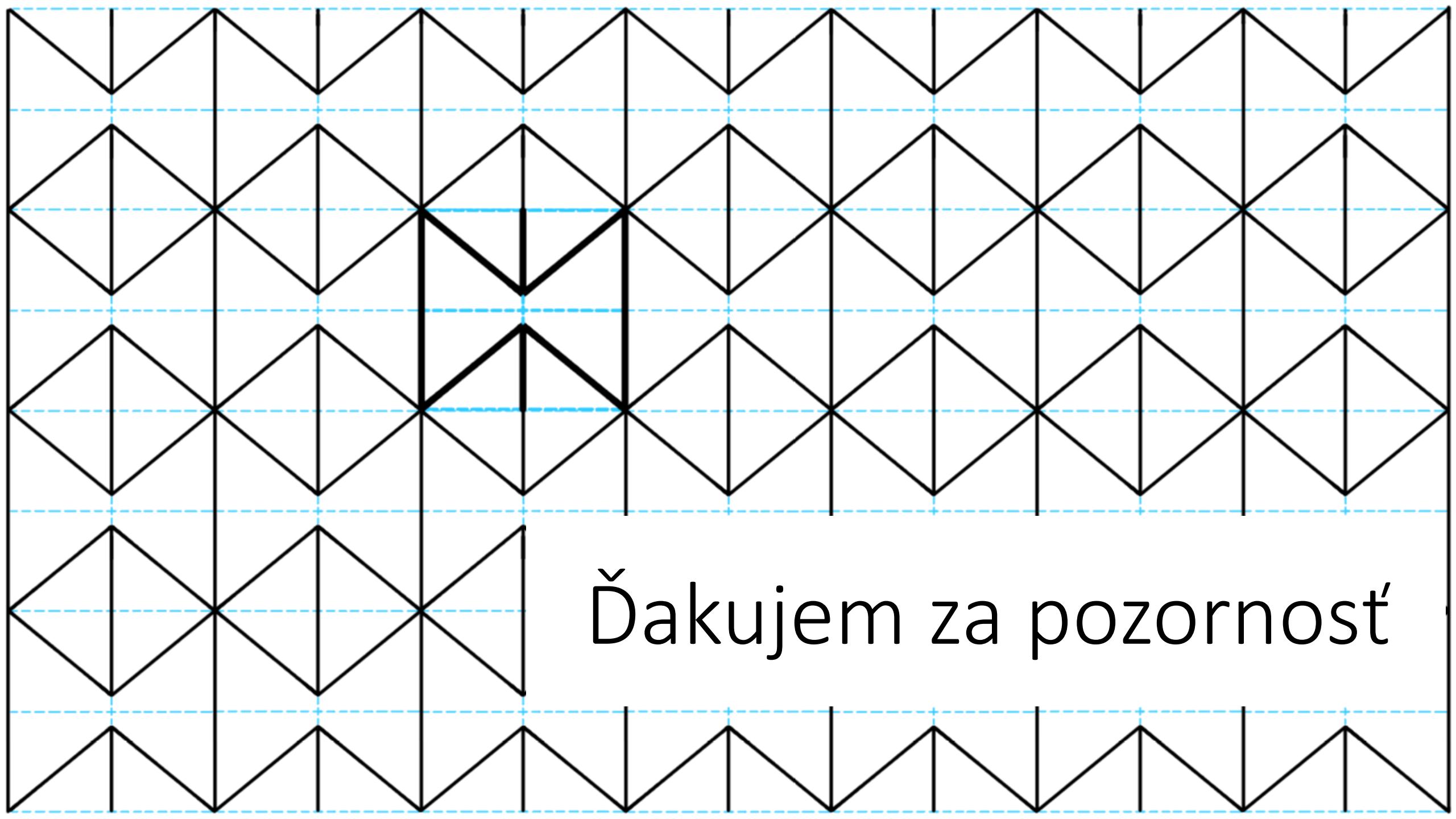


Uzel	x [~m]	y [~m]	z [~m]	u [~m]	w [~m]	phi [~rad]
1	0	0	10	0.89027316	0	0
2	0	0	0	0.89027316	0	0
3	10	0	8.9038	0	1	0

Zanedbanie λ







Ďakujem za pozornosť