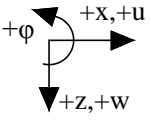
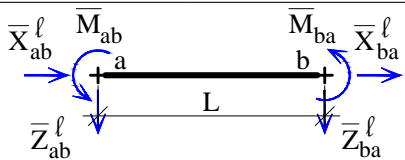
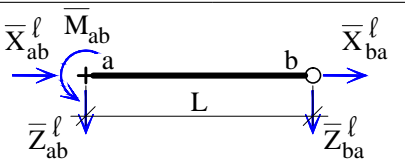
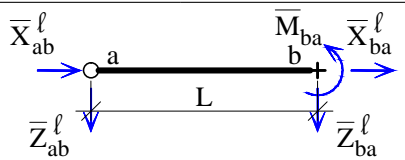
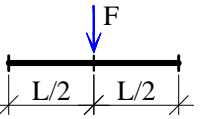
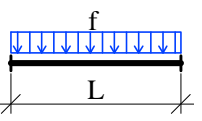
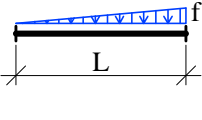
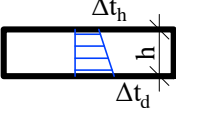
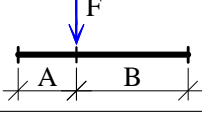
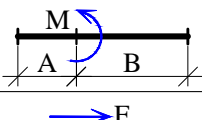
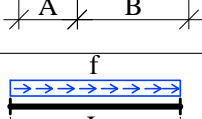
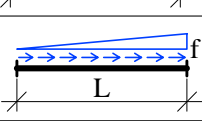
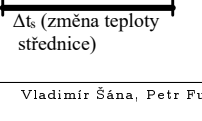
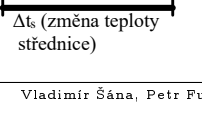


DEFORMAČNÍ METODA – Celkové koncové momenty a síly

	prut typu V-V	
$k = \frac{2EI}{L}$	$M_{ab} = \bar{M}_{ab} + k \left(2\varphi_a + \varphi_b + 3 \frac{w_b^l - w_a^l}{L} \right)$ $Z_{ab}^l = \bar{Z}_{ab}^l - \frac{k}{L} \left(3\varphi_a + 3\varphi_b + 6 \frac{w_b^l - w_a^l}{L} \right)$ $X_{ab}^l = \bar{X}_{ab}^l - n(u_b^l - u_a^l)$	$M_{ba} = \bar{M}_{ba} + k \left(\varphi_a + 2\varphi_b + 3 \frac{w_b^l - w_a^l}{L} \right)$ $Z_{ba}^l = \bar{Z}_{ba}^l + \frac{k}{L} \left(3\varphi_a + 3\varphi_b + 6 \frac{w_b^l - w_a^l}{L} \right)$ $X_{ba}^l = \bar{X}_{ba}^l + n(u_b^l - u_a^l)$
	prut typu V-K	
$n = \frac{EA}{L}$	$M_{ab} = \bar{M}_{ab} + k \left(1,5\varphi_a + 1,5 \frac{w_b^l - w_a^l}{L} \right)$ $Z_{ab}^l = \bar{Z}_{ab}^l - \frac{k}{L} \left(1,5\varphi_a + 1,5 \frac{w_b^l - w_a^l}{L} \right)$ $X_{ab}^l = \bar{X}_{ab}^l - n(u_b^l - u_a^l)$	<p style="text-align: center;">x</p> $Z_{ba}^l = \bar{Z}_{ba}^l + \frac{k}{L} \left(1,5\varphi_a + 1,5 \frac{w_b^l - w_a^l}{L} \right)$ $X_{ba}^l = \bar{X}_{ba}^l + n(u_b^l - u_a^l)$
	prut typu K-V	
x	$Z_{ab}^l = \bar{Z}_{ab}^l - \frac{k}{L} \left(1,5\varphi_b + 1,5 \frac{w_b^l - w_a^l}{L} \right)$ $X_{ab}^l = \bar{X}_{ab}^l - n(u_b^l - u_a^l)$	$M_{ba} = \bar{M}_{ba} + k \left(1,5\varphi_b + 1,5 \frac{w_b^l - w_a^l}{L} \right)$ $Z_{ba}^l = \bar{Z}_{ba}^l + \frac{k}{L} \left(1,5\varphi_b + 1,5 \frac{w_b^l - w_a^l}{L} \right)$ $X_{ba}^l = \bar{X}_{ba}^l + n(u_b^l - u_a^l)$
Transformace koncových sil		
	$X^g = X^l \cos \alpha - Z^l \sin \alpha$ $Z^g = X^l \sin \alpha + Z^l \cos \alpha$	
Transformace styčnickových posunů		
	$u^l = u^g \cos \alpha + w^g \sin \alpha$ $w^l = -u^g \sin \alpha + w^g \cos \alpha$	

DEFORMAČNÍ METODA – Koncové momenty a síly od prutového zatížení

	prut typu V-V	prut typu V-K	prut typu K-V
			
	$\bar{M}_{ab} = \frac{FL}{8}$ $\bar{M}_{ba} = -\frac{FL}{8}$	$\bar{M}_{ab} = \frac{3}{16}FL$ x	x $\bar{M}_{ba} = -\frac{3}{16}FL$
	$\bar{Z}_{ab} = -\frac{F}{2}$ $\bar{Z}_{ba} = -\frac{F}{2}$	$\bar{Z}_{ab} = -\frac{11F}{16}$ $\bar{Z}_{ba} = -\frac{5F}{16}$	$\bar{Z}_{ab} = -\frac{5F}{16}$ $\bar{Z}_{ba} = -\frac{11F}{16}$
	$\bar{M}_{ab} = \frac{fL^2}{12}$ $\bar{M}_{ba} = -\frac{fL^2}{12}$	$\bar{M}_{ab} = \frac{fL^2}{8}$ x	x $\bar{M}_{ba} = -\frac{fL^2}{8}$
	$\bar{Z}_{ab} = -\frac{fL}{2}$ $\bar{Z}_{ba} = -\frac{fL}{2}$	$\bar{Z}_{ab} = -\frac{5fL}{8}$ $\bar{Z}_{ba} = -\frac{3fL}{8}$	$\bar{Z}_{ab} = -\frac{3fL}{8}$ $\bar{Z}_{ba} = -\frac{5fL}{8}$
	$\bar{M}_{ab} = \frac{fL^2}{30}$ $\bar{M}_{ba} = -\frac{fL^2}{20}$	$\bar{M}_{ab} = \frac{7fL^2}{120}$ x	x $\bar{M}_{ba} = -\frac{fL^2}{15}$
	$\bar{Z}_{ab} = -\frac{3fL}{20}$ $\bar{Z}_{ba} = -\frac{7fL}{20}$	$\bar{Z}_{ab} = -\frac{27fL}{120}$ $\bar{Z}_{ba} = -\frac{33fL}{120}$	$\bar{Z}_{ab} = -\frac{fL}{10}$ $\bar{Z}_{ba} = -\frac{2fL}{5}$
	$\bar{M}_{ab} = EI\alpha_t \frac{\Delta t_d - \Delta t_h}{h}$ $\bar{M}_{ba} = -EI\alpha_t \frac{\Delta t_d - \Delta t_h}{h}$	$\bar{M}_{ab} = \frac{3}{2}EI\alpha_t \frac{\Delta t_d - \Delta t_h}{h}$ x	x $\bar{M}_{ba} = -\frac{3}{2}EI\alpha_t \frac{\Delta t_d - \Delta t_h}{h}$
	$\bar{Z}_{ab} = 0$ $\bar{Z}_{ba} = 0$	$\bar{Z}_{ab} = -\frac{3EI}{2L}\alpha_t \frac{\Delta t_d - \Delta t_h}{h}$ $\bar{Z}_{ba} = \frac{3EI}{2L}\alpha_t \frac{\Delta t_d - \Delta t_h}{h}$	$\bar{Z}_{ab} = \frac{3EI}{2L}\alpha_t \frac{\Delta t_d - \Delta t_h}{h}$ $\bar{Z}_{ba} = -\frac{3EI}{2L}\alpha_t \frac{\Delta t_d - \Delta t_h}{h}$
	$\bar{M}_{ab} = \frac{FAB^2}{L^2}$ $\bar{M}_{ba} = -\frac{FA^2B}{L^2}$	$\bar{M}_{ab} = \frac{FAB}{2L^2}(B+L)$ x	x $\bar{M}_{ba} = -\frac{FAB}{2L^2}(A+L)$
	$\bar{Z}_{ab}, \bar{Z}_{ba}$ se dopočítají z podmínek rovnováhy prutu		
	$\bar{M}_{ab} = \frac{MB}{L^2}(2L-3B)$ $\bar{M}_{ba} = \frac{MA}{L^2}(2L-3A)$	$\bar{M}_{ab} = \frac{M}{2L^2}(L^2-3B^2)$ x	x $\bar{M}_{ba} = \frac{M}{2L^2}(L^2-3A^2)$
	$\bar{Z}_{ab}, \bar{Z}_{ba}$ se dopočítají z podmínek rovnováhy prutu		
	$\bar{X}_{ab} = -\frac{FB}{L}$ $\bar{X}_{ba} = -\frac{FA}{L}$	$\bar{X}_{ab} = -\frac{FB}{L}$ $\bar{X}_{ba} = -\frac{FA}{L}$	$\bar{X}_{ab} = -\frac{FB}{L}$ $\bar{X}_{ba} = -\frac{FA}{L}$
	$\bar{X}_{ab} = -\frac{fL}{2}$ $\bar{X}_{ba} = -\frac{fL}{2}$	$\bar{X}_{ab} = -\frac{fL}{2}$ $\bar{X}_{ba} = -\frac{fL}{2}$	$\bar{X}_{ab} = -\frac{fL}{2}$ $\bar{X}_{ba} = -\frac{fL}{2}$
	$\bar{X}_{ab} = -\frac{fL}{6}$ $\bar{X}_{ba} = -\frac{fL}{3}$	$\bar{X}_{ab} = -\frac{fL}{6}$ $\bar{X}_{ba} = -\frac{fL}{3}$	$\bar{X}_{ab} = -\frac{fL}{6}$ $\bar{X}_{ba} = -\frac{fL}{3}$
	$\bar{X}_{ab} = EA\alpha_t\Delta t_s$ $\bar{X}_{ba} = -EA\alpha_t\Delta t_s$	$\bar{X}_{ab} = EA\alpha_t\Delta t_s$ $\bar{X}_{ba} = -EA\alpha_t\Delta t_s$	$\bar{X}_{ab} = EA\alpha_t\Delta t_s$ $\bar{X}_{ba} = -EA\alpha_t\Delta t_s$