

Microstructurally-Informed Random Field Description: Case Study on Chaotic Masonry

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Motivation: Analysis of a historic masonry wall



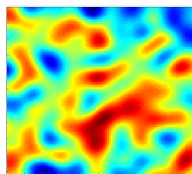
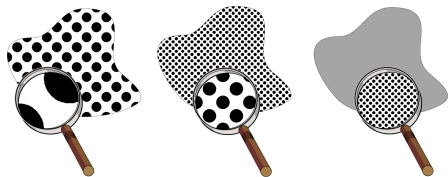
- Key issues
 - **Heterogeneity** and **non-uniformity** of the structure
 - Size of constituents **not negligible** with respect to structural length
 - **Random** morphology of the material
- Available modeling concepts
 - ① Homogenization approaches
 - ② Stochastic media theories

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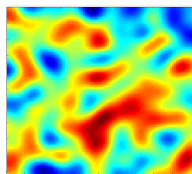
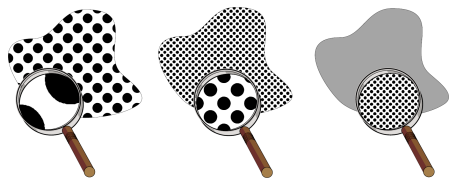
Motivation: Homogenization vs random fields



- **Rapidly oscillating** coefficients
- Assumes **scale separation**
- Periodic unit cell (PUC)
- Random materials \rightarrow SEPUC
- Explicit treatment of heterogeneity
(ZEMAN & ŠEJNOHA, MSMSE, 2007)

- **Random** coefficients
- No **a-priory** scale separation
- Random field construction
- Randomness is “for free”
- **Link with microstructure?**

Motivation: Homogenization vs random fields



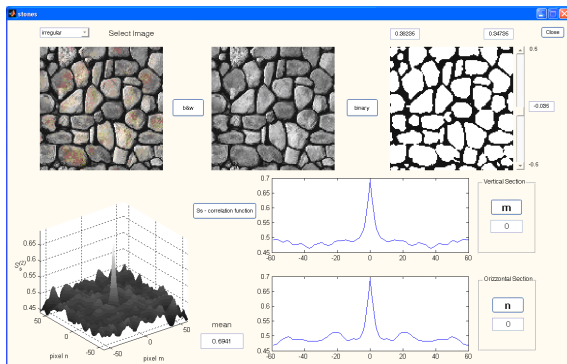
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- 1 Quantification of random morphology
- 2 Statistics of structural response
 - Improved perturbation technique
 - Karhunen-Loève expansion
 - Hashin-Shtrikman approach
- 3 Numerical example
- 4 Conclusions

Quantification of random morphology

- Elementary geometrical descriptors of random media
 - One-point correlation function $S_s^{(1)} \equiv \gamma_s$ (volume fraction)
 - Two-point correlation function $S_s^{(2)}(m, n)$
- STONES environment (FALSONE & LOMBARDO, 2006)



- Consider a **discrete** binary random field $\chi_s : \Omega \times \mathcal{S} \rightarrow \{0, 1\}$

$$\chi_s(\mathbf{x}, \theta) = \begin{cases} 1 & \text{if } \mathbf{x} \in \text{stone}(\theta) \\ 0 & \text{if } \mathbf{x} \in \text{mortar}(\theta) \end{cases} \quad \begin{aligned} \mathbb{E}[\chi_s(\mathbf{x})] &= \gamma_s \\ \mathbb{E}[\chi_s(\mathbf{x})\chi_s(\mathbf{y})] &= S_s^{(2)}(\mathbf{x} - \mathbf{y}) \end{aligned}$$

- For a general binary field $f : \Omega \times \mathcal{S} \rightarrow \mathbb{R}$

$$f(\mathbf{x}, \theta) = \begin{cases} f^{(s)} & \text{if } \mathbf{x} \in \text{stone}(\theta) \\ f^{(m)} & \text{if } \mathbf{x} \in \text{mortar}(\theta) \end{cases}$$

- Basic statistical characterization

$$\begin{aligned} \mathbb{E}[f(\mathbf{x})] &= \gamma_s f^{(s)} + (1 - \gamma_s) f^{(m)} \\ R_{fg}(\mathbf{x} - \mathbf{y}) &= \left(S_s^{(2)}(\mathbf{x} - \mathbf{y}) - \gamma_s^2 \right) \left(f^{(s)} - f^{(m)} \right) \left(g^{(s)} - g^{(m)} \right) \end{aligned}$$

- Rigorous **microstructure-based** description

- Elasticity problem on Ω with **stochastic material data**

$$\mathbf{C}(\mathbf{x}, \theta) = \chi_s(\mathbf{x}, \theta)\mathbf{C}^{(s)} + (1 - \chi_s(\mathbf{x}, \theta))\mathbf{C}^{(m)}$$

- Discretization of Ω by N_e elements ($2h \lesssim$ **correlation length**)
- **Midpoint discretization** of random field:

$$\boldsymbol{\chi}_s^h(\theta) = [\chi_{s,1}^h(\theta), \chi_{s,2}^h(\theta) \dots, \chi_{s,N_e}^h(\theta)]^T \in \{0, 1\}^{N_e}$$

- Discretized FEM equations: $\mathbf{K}(\boldsymbol{\chi}_s^h(\theta))\mathbf{u}^h(\theta) = \mathbf{F}$
- Elementary **statistics of displacements**

$$\mathbf{A} \mathbb{E}[\mathbf{u}^h] = \mathbf{F}$$

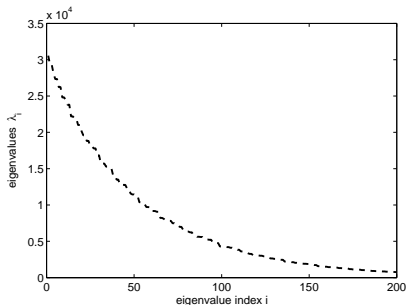
where

$$\mathbf{A} = \mathbf{K}_0 - \sum_{i=1}^{N_e} \sum_{j=1}^{N_e} \mathbf{K}'_i (\mathbf{K}_0)^{-1} \mathbf{K}'_j \mathbb{E}[\chi_{s,i} \chi_{s,j}]$$

- Karhunen-Loève expansion of a stationary random field $g(\mathbf{x}, \theta)$

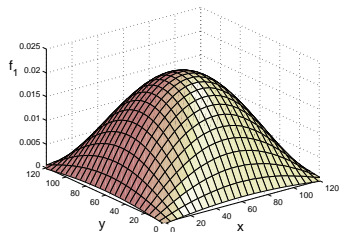
$$g(\mathbf{x}, \theta) = \mathbb{E}[g] + \sum_{i=1}^M \sqrt{\lambda_i} f_i(\mathbf{x}) \xi_i(\theta),$$

$$\int_{\Omega} R_g(\mathbf{x} - \mathbf{y}) f_i(\mathbf{y}) d\mathbf{y} = \lambda_i f_i(\mathbf{x}) \quad \xi_i(\theta) = \frac{1}{\sqrt{\lambda_i}} \int_{\Omega} (g(\mathbf{x}, \theta) - \mathbb{E}[g]) f_i(\mathbf{x}) d\mathbf{x}$$

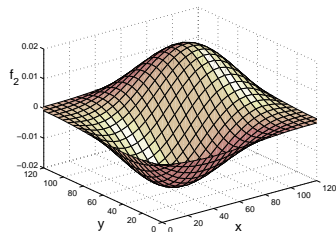


Statistics of structural response

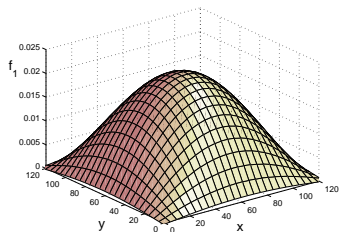
Karhunen-Loève expansion



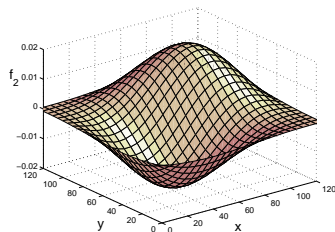
$i = 1$



$i = 2$



$i = 12$

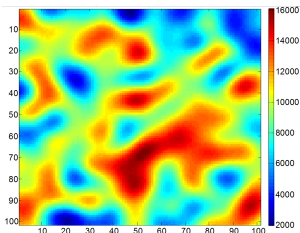


$i = 24$

Statistics of structural response

Karhunen-Loève expansion

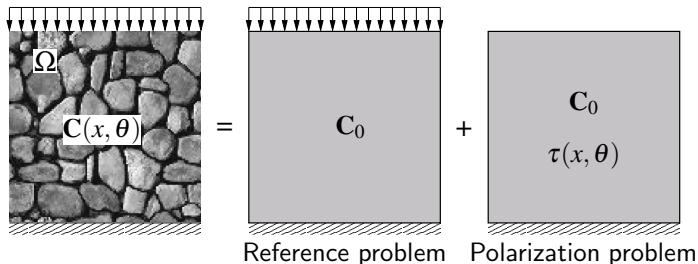
- Spatial dimensional x is accurately captured
- Stochastic dimension θ : Truncated **Gaussian** variables



- Evaluation of statistics: Monte-Carlo integration

$$\mathbb{E}[\mathbf{u}] \approx \frac{1}{N_s} \sum_{s=1}^{N_s} \mathbf{u}^h(\theta_i)$$

with $N_s = 10,000$



- Reference body Ω with stiffness \mathbf{C}_0
- Stress equivalence condition

$$\boldsymbol{\sigma}(x, \theta) = \mathbf{C}(x, \theta)\boldsymbol{\varepsilon}(x, \theta) = \mathbf{C}_0\boldsymbol{\varepsilon}(x, \theta) + \boldsymbol{\tau}(x, \theta)$$

- Approximate solution of reference problem using FEM

$$\boldsymbol{\varepsilon}_0^h(\mathbf{x}), \mathbf{G}_0^h(\mathbf{x}, \mathbf{y}) = \mathbf{N}_u^h(\mathbf{x})(\mathbf{K}_0^h)^{-1}\mathbf{B}^{h\top}(\mathbf{y}), \boldsymbol{\Gamma}_0^h(\mathbf{x}, \mathbf{y}) = \mathbf{B}^h(\mathbf{x})(\mathbf{K}_0^h)^{-1}\mathbf{B}^{h\top}(\mathbf{y})$$

Statistics of structural response

Hashin-Shtrikman approach: Polarization problem

- Polarization stress: $\boldsymbol{\tau}^h(\mathbf{x}, \theta) = \mathbf{N}^h(\mathbf{x}) (\chi_1(\mathbf{x}, \theta) \mathbf{d}_1^h + \chi_2(\mathbf{x}, \theta) \mathbf{d}_2^h)$
- Discretized version of H-S variational principles

$$\mathbf{K}_i^h \mathbf{d}_i^h + \sum_j \mathbf{K}_{ij}^h \mathbf{d}_j^h = \mathbf{R}_i^h$$

$$\mathbf{K}_i^h = \int_{\Omega} \gamma_i(\mathbf{x}) \mathbf{N}^{h\top}(\mathbf{x}) [\mathbf{C}_i - \mathbf{C}_0]^{-1} \mathbf{N}^h(\mathbf{x}) \, d\mathbf{x}$$

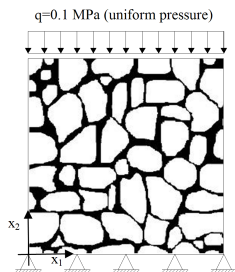
$$\mathbf{K}_{ij}^h = \int_{\Omega} \mathbf{N}^{h\top}(\mathbf{x}) \int_{\Omega} S_{ij}^{(2)}(\mathbf{x} - \mathbf{y}) \boldsymbol{\Gamma}_0^h(\mathbf{x}, \mathbf{y}) \mathbf{N}^h(\mathbf{y}) \, d\mathbf{x} \, d\mathbf{y}$$

$$\mathbf{R}_i^h = \int_{\Omega} \gamma_i(\mathbf{x}) \mathbf{N}^{h\top}(\mathbf{x}) \boldsymbol{\varepsilon}_0^h(\mathbf{x}) \, d\mathbf{x}$$

- Statistics of the solution:

$$\mathbb{E}[\mathbf{u}^h(\mathbf{x})] = \mathbf{u}_0^h(\mathbf{x}) - \int_{\Omega} \mathbf{G}_0^h(\mathbf{x}, \mathbf{y}) \mathbf{N}^h(\mathbf{y}) (\gamma_1 \mathbf{d}_1^h + \gamma_2 \mathbf{d}_2^h) \, d\mathbf{y}$$

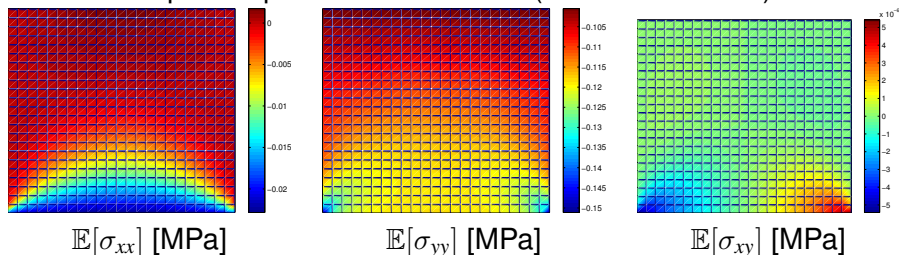
Numerical example



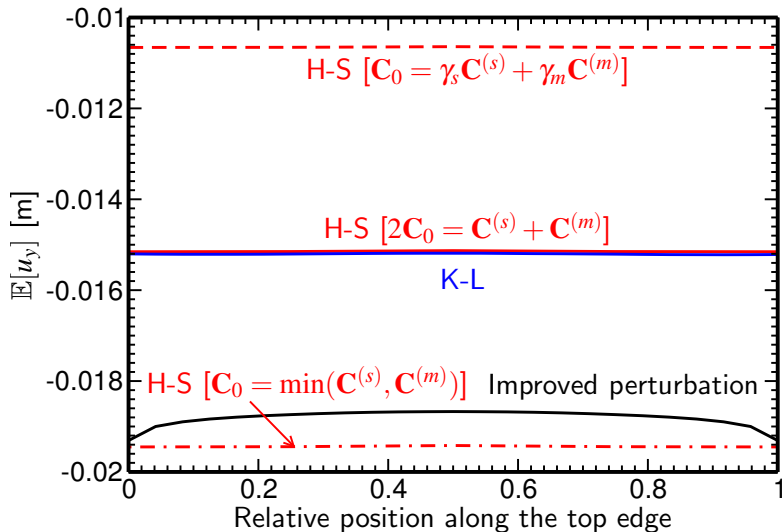
Phase	E [MPa]	ν [-]
Stone	12 500	0.2
Mortar	1 200	0.3

Q1/(Q0) elements

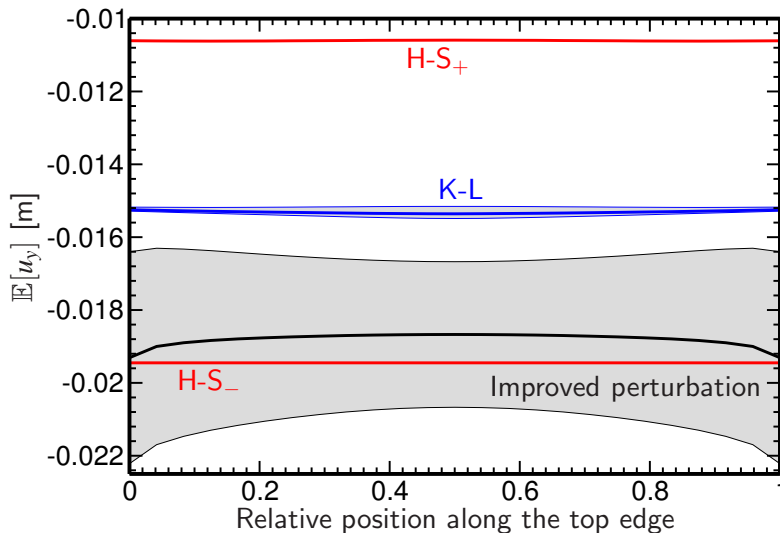
Improved perturbation method (25×25 elements)



Numerical example



Numerical example



Conclusions

- Spatial correlation of a random field can be directly obtained from samples of microstructure
- Improved perturbation method seems to fully utilize second-order data, but it inconsistent with the H-S bounds
- Karhunen-Loeve expansion needs a large number of terms for realistic structures
- Results of Hashin-Shtrikman method **strongly depend** on the choice of reference media
- Need for a rational construction of **non-Gaussian** fields with prescribed correlation structure

Additional info available at

<http://www.arxiv.org/abs/0811.0972>