Finite Element Formulation for One-Dimensional Non-stationary Heat Conduction Problems

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FEM FORMULATION FOR NO-STATIONARY HEAT TRANSFER PROBLEM

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Transport equation:

 \blacksquare Fourier's law: heat flux in a material point $x\in \Omega$

$$\boldsymbol{q}(x,t) = -\lambda(\boldsymbol{x}) \operatorname{grad} T(\boldsymbol{x},t)$$

Balance equation:

 \blacksquare Energy conservation equation in a volume element Ω

$$-\mathrm{div}\left(-\lambda(\boldsymbol{x})\,\mathrm{grad}T(\boldsymbol{x},t)\right) = \rho(x)C(x)\,\,\frac{\partial T(\boldsymbol{x},t)}{\partial t},\qquad \boldsymbol{x},\in\Omega$$

where $\lambda(\boldsymbol{x})$ is the conductivity coefficient [W·m⁻¹K⁻¹], $\rho(\boldsymbol{x})$ [kg·m⁻³] is the volume weight, and $C(\boldsymbol{x})$ [J·kg⁻¹·K⁻¹] is the specific heat (capacity).



STRONG FORM FOR 1D PROBLEM

Derivation of non-stationary heat transfer equation:



For 1D problem - partial differential equation:

$$\frac{\partial}{\partial x} \left(\lambda(x) \frac{\partial T(x,t)}{\partial x} \right) + \overline{Q}(x,t) = \rho(x) C(x) \ \frac{\partial T(x,t)}{\partial t}$$

Initial condition:

$$T(x,t=0) = T_0(x,t), \qquad x \in \Omega$$



DERIVATION OF HEAT TRANSFER EQUATION

Boundary conditions:

Dirichlet b.c. - prescribed temperature on the boundary:

$$T(x,t) = \overline{T}(x,t) \qquad x \in \Gamma_T$$

• Neumann b.c - prescribed flux on the boundary:

$$q(x,t) = \overline{q}(x,t)$$
 $x \in \Gamma_{qp}$

Cauchy - Newton b.c. - heat transfer on the boundary:

$$q(x,t) = \alpha(x) \left(T(x,t) - T_{\infty}(x,t) \right) \qquad x \in \Gamma_{qc}$$

 $\alpha(x)$ is the heat transfer coefficient [Wm⁻²K⁻¹], $T_{\infty}(x,t)$ is the ambient temperature Non-linear b.c. (Newton) - heat radiation on the boundary:

$$q(x,t) = \varepsilon(x,t)\sigma(x,t) \left(T^4(x,t) - T^4_{\infty}(x,t)\right) \qquad x \in \Gamma_{qr}$$

where $\varepsilon(x,t)$ is the rate of the surface radiation related to a black body radiation $(0 < \varepsilon < 1)$, $\sigma(x,t) = 5,67 \cdot 10^{-8} \text{ Wm}^{-2} \text{K}^{-4}$ is the Stefan-Boltzmann constant, and $T_{\infty}(x,t)$ is the ambient temperature (temperature of a radiator).



WEIGHTED RESIDUAL METHOD

Weighted residual method (Galerkin method):

• We are looking for a solution T(x,t) smooth enough, which fulfills $x \in \Omega$:

$$\frac{\partial}{\partial x} \left(\lambda(x) \frac{\partial T(x,t)}{\partial x} \right) + \overline{Q}(x,t) - \rho(x)C(x) \ \frac{\partial T(x,t)}{\partial t} = 0$$

• Initial condition: for t = 0:

$$T(x,t=0) = T_0(x,t), \qquad x \in \Omega$$

• for $x \in \Gamma_T$:

$$T(x,t) = \overline{T}(x,t)$$

• for $x\in\Gamma_q$: $q(x,t)=-\lambda(x)\frac{\partial T(x,t)}{\partial x}\boldsymbol{n}(x,t)=\overline{q}(x,t),$

where:

• for $x \in \Gamma_{qp}$: $\overline{q}(x,t)$ is prescribed • for $x \in \Gamma_{qc}$: $\overline{q}(x,t) = \alpha(x) \left(T(x,t) - T_{\infty}(x,t)\right)$ • for $x \in \Gamma_{qr}$: $\overline{q}(x,t) = \varepsilon(x,t)\sigma(x,t) \left(T^4(x,t) - T^4_{\infty}(x,t)\right)$ (it is avoided in the derivation)



WEIGHTED RESIDUAL METHOD

Weighted residual method (Galerkin method):

• For an arbitrary weight function δT so that $\delta T(x,t) = 0$ for $x \in \Gamma_T$, it holds:

$$\int_{\Omega} \left\{ \delta T(x,t) \left(\frac{\partial}{\partial x} \left(\lambda(x) \frac{\partial T(x,t)}{\partial x} \right) + \overline{Q}(x,t) - \rho(x)C(x) \ \frac{\partial T(x,t)}{\partial t} \right) \mathrm{d}\Omega \right\} = 0, \qquad x \in \Omega$$

Integration by parts, we get:

$$\begin{split} \int_{\Gamma} \delta T(x,t)\lambda(x) \frac{\mathrm{d}T(x,t)}{\mathrm{d}x} \boldsymbol{n}(x,t)\mathrm{d}\Gamma & - \int_{\Omega} \frac{\mathrm{d}\delta T(x,t)}{\mathrm{d}x}\lambda(x) \frac{\mathrm{d}T(x,t)}{\mathrm{d}x}\mathrm{d}\Omega + \int_{\Omega} \delta T(x,t)\overline{Q}(x,t)\mathrm{d}\Omega \\ & - \int_{\Omega} \delta T(x,t)\rho(x)C(x) \; \frac{\partial T(x,t)}{\partial t}\mathrm{d}\Omega = 0 \end{split}$$

0

where the integral on the boundary:

$$\int_{\Gamma} \delta T(x,t)\lambda(x) \frac{\mathrm{d}T(x,t)}{\mathrm{d}x} \boldsymbol{n}(x,t)\mathrm{d}\Gamma = \int_{\Gamma_{T}} \widetilde{\delta T(x,t)} \lambda(x) \frac{\mathrm{d}T(x,t)}{\mathrm{d}x} \boldsymbol{n}(x,t)\mathrm{d}\Gamma + \int_{\Gamma_{q}} \delta T(x,t) \underbrace{\lambda(x) \frac{\mathrm{d}T(x,t)}{\mathrm{d}x} \boldsymbol{n}(x,t)}_{=-q(x,t)} \mathrm{d}\Gamma$$



FEM FORMULATION FOR NO-STATIONARY HEAT TRANSFER PROBLEM

It follows:

$$\int_{\Gamma_q} \delta T(x,t) q(x,t) \mathrm{d}\Gamma = \int_{\Gamma_{qp}} \delta T(x,t) \overline{q}(x,t) \mathrm{d}\Gamma + \int_{\Gamma_{qc}} \delta T(x,t) \alpha(x) \left(T(x,t) - T_{\infty}(x,t) \right) \mathrm{d}\Gamma$$

Weak form:

$$\begin{split} &\int_{\Omega} \frac{\partial \delta T(x,t)}{\partial x} \lambda \frac{\partial T(x,t)}{\partial x} \mathrm{d}\Omega + \int_{\Gamma_{qc}} \delta T(x,t) \alpha T(x,t) \mathrm{d}\Gamma + \int_{\Omega} \delta T(x,t) \rho C \ \frac{\partial T(x,t)}{\partial t} \mathrm{d}\Omega = \\ &= \int_{\Gamma_{qp}} \delta T(x,t) \overline{q}(x,t) \mathrm{d}\Gamma + \int_{\Gamma_{qc}} \delta T(x,t) \alpha T_{\infty}(x,t) \mathrm{d}\Gamma + \int_{\Omega} \delta T(x,t) \overline{Q}(x,t) \mathrm{d}\Omega, \end{split}$$

We are looking for such an admissible trial solution T(x,t) which satisfies the above formulation.



FINITE ELEMENT METHOD

Finite Element Method:

• The temperature function T is approximated in each element in the following shape:

 $T^{e}(x,t) \approx \boldsymbol{N}^{e}(x)\boldsymbol{r}^{e}(t), \ \mathrm{grad}T^{e}(x,t) \approx \boldsymbol{B}^{e}(x)\boldsymbol{r}^{e}(t), \ \delta T^{e}(x,t) \approx \boldsymbol{N}^{e}(x)\boldsymbol{w}^{e}(t), \ \mathrm{grad}\delta T^{e}(x,t) \approx \boldsymbol{B}^{e}(x)\boldsymbol{w}^{e}(t)$

FEM FORMULATION FOR NO-STATIONARY HEAT TRANSFER PROBLEM

Introducing approximations of trial solution and weight function into the weak form (for all $w^e(t)$ that $w^e(t) = 0$ on Γ_T), we obtain the following equation:



FEM DISCRETIZATION



Finite Element Method:

If local vectors r^e , w^e are expanded into global vectors of nodal values r, w, we can write:

$$\boldsymbol{w}^{\mathrm{T}}\left(\sum_{e=1}^{n} \hat{\boldsymbol{K}}^{e} \boldsymbol{r} + \sum_{e=1}^{n} \hat{\boldsymbol{C}}^{e} \frac{\mathrm{d}\boldsymbol{r}}{\mathrm{d}t} - \sum_{e=1}^{n} \hat{\boldsymbol{f}}^{e}\right) = 0$$

Finaly, we have:

$$Kr + C \frac{\mathrm{d}r}{\mathrm{d}t} = f$$

- Note: Two basic approaches of weak form solution:
 - Discretization of the whole "time-space" domain time-spatial finite elements
 - Separate spatial discretization and time disretization (time integration)



FINITE ELEMENT METHOD

Time integration:

$$Kr + C\dot{r} = f \tag{1}$$

- Time integration we consider time intervals, where $\Delta t = t_i t_{i-1}$
- Known solution in previous time t_{i-1} : r_{i-1}
- Linear approximation of trial solution in time *r*:

$$\boldsymbol{r}(t) = \tau \boldsymbol{r}_i + (1 - \tau) \boldsymbol{r}_{i-1},\tag{2}$$

where $\tau = (t - t_{i-1})/\Delta t$

The same linear approximation of right-hand side vector *f*:

$$\boldsymbol{f}(t) = \tau \boldsymbol{f}_i + (1 - \tau) \boldsymbol{f}_{i-1}, \tag{3}$$

Time derivative of the vector of nodal temperatures

$$\frac{\mathrm{d}\boldsymbol{r}}{\mathrm{d}t} = \frac{1}{\Delta t} (\boldsymbol{r}_i - \boldsymbol{r}_{i-1}) \tag{4}$$

Introduction of equations (2), (3), and (4) into the final system of equations (1), we obtain the system of linear algebraic equations:

$$\left[\boldsymbol{K}\boldsymbol{\tau} + \frac{\boldsymbol{C}}{\Delta t}\right]\boldsymbol{r}_{i} = \boldsymbol{f}_{i-1}(1-\tau) + \boldsymbol{f}_{i}\boldsymbol{\tau} + \left[\frac{\boldsymbol{C}}{\Delta t} - \boldsymbol{K}(1-\tau)\right]\boldsymbol{r}_{i-1}$$



- English course of "Numerical analysis of structures" by J. Zeman (jan.zeman@fsv.cvut.cz)
- Czech course of "Numerická analýza konstrukcí" (Numerical analysis of structures) by B. Patzák (borek.patzak@fsv.cvut.cz)
- J. Fish and T. Belytschko: A First Course in Finite Elements, John Wiley & Sons, 2007

