Finite Element Formulation for Two-Dimensional Heat Conduction Problem

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1 MOTIVATION

- BASIC TERMS AND QUANTITIES
 Differential equation of heat transfer
- **3** Weighted residual method

4 WEAK FORM

5 FEM DISCRETIZATION



INTRODUCTION

- Stationary 2D problem:
- \blacksquare The derivation similar to the 1D problem extension to 2D (x,y)
- Heat transfer (conduction):
 - function of temperature distribution $T(\boldsymbol{x},\boldsymbol{y})$ [K]
 - solution procedure:

$$\begin{array}{c} \text{Differential equation} \\ \rightarrow \quad \text{weak form} \\ \rightarrow \quad \text{FEM discretization} \end{array}$$

Temperature gradient:

$$\boldsymbol{\nabla}T(x,y) = \operatorname{grad}T(x,y) = \left[\frac{\partial T(x,y)}{\partial x}, \frac{\partial T(x,y)}{\partial y}\right]^{\mathrm{T}}$$

• Heat flux $q_n(x, y)$ is an amount of heat energy, which is transferred through a unit area A $\overline{[1m^2]}$ with outer normal n per time unit t [s]:

$$\boldsymbol{q}_n(x,y) = \frac{Q(x,y)}{A\cdot t}\boldsymbol{n}(x,y), \qquad [\mathrm{Wm}^{-2}]$$



• Heat flux inside a body $(x, y \in \Omega)$ can be decomposed into two directions:

 $\boldsymbol{q} = \left[q_x(x,y), q_y(x,y)\right]^{\mathrm{T}}$

Transport equation:

• Fourier's law: heat flux in an internal body point (material point) $x, y \in \Omega$

$$\boldsymbol{q}(x,y) = -\boldsymbol{\lambda}(x,y) \, \boldsymbol{\nabla} T(x,y),$$

where $\lambda(x, y)$ is the matrix of heat conduction coefficients [Wm⁻¹K⁻¹] Balance equation:

• Energy balance in a volume element Ω

$$\boldsymbol{\nabla}^{\mathrm{T}}\left(-\boldsymbol{\lambda}(\boldsymbol{x})\,\boldsymbol{\nabla}T(\boldsymbol{x})\right) = 0,$$

where $\boldsymbol{x} = (x, y)$



DERIVATION OF HEAT TRANSFER EQUATION

Derivation of heat transfer equation:

Inside a body $(\boldsymbol{x} \in \Omega)$:

$$\begin{aligned} q_x(x,y)\Delta y &- q_x(x + \Delta x, y)\Delta y & (\to x) \\ + q_y(x,y)\Delta x &- q_y(x,y + \Delta y)\Delta x & (\uparrow y) \\ &+ \overline{Q}\left(x + \frac{\Delta x}{2}, y + \frac{\Delta y}{2}\right)\Delta x\Delta y = 0. \end{aligned}$$

• Dividing by $\Delta x \Delta y$, and for the limit limitním přechodem $\Delta x \to 0$ a $\Delta y \to 0$, it follows

$$-\frac{\partial q_x}{\partial x}(x,y) - \frac{\partial q_y}{\partial y}(x,y) + \overline{Q}(x,y) = 0,$$

which can be written in matrix form

$$-\begin{bmatrix} \frac{\partial}{\partial x} & \frac{\partial}{\partial y} \end{bmatrix} \begin{bmatrix} q_x(x,y) \\ q_y(x,y) \end{bmatrix} + \overline{Q}(x,y) = 0$$

and:

$$-\boldsymbol{\nabla}^{\mathrm{T}}\boldsymbol{q}(\boldsymbol{x}) + \overline{Q}(\boldsymbol{x}) = 0$$



Derivation of heat transfer equation:

Introducing of Fourier's law , we obtain a partial differential equation of second order for heat transfer:

$$\boldsymbol{\nabla}^{\mathrm{T}}\left(\boldsymbol{\lambda}(\boldsymbol{x})\boldsymbol{\nabla}T(\boldsymbol{x})\right) + \overline{Q}(\boldsymbol{x}) = 0$$

 $oldsymbol{\lambda}(oldsymbol{x})$ is the material conductivity matrix:

$$oldsymbol{\lambda}(oldsymbol{x}) = \left[egin{array}{cc} \lambda_{xx}(x,y), & \lambda_{xy}(x,y) \ \lambda_{yx}(x,y), & \lambda_{yy}(x,y) \end{array}
ight]$$

The matrix $(\lambda_{xy} = \lambda_{yx})$ is symmetric and positive definite. For isotropic material reads:

$$oldsymbol{\lambda}(oldsymbol{x}) = \left[egin{array}{cc} \lambda(oldsymbol{x}), & 0 \ 0, & \lambda(oldsymbol{x}) \end{array}
ight]$$



DERIVATION OF HEAT TRANSFER EQUATION

Boundary conditions:

Dirichlet b.c. - prescribed temperature on the boundary:

$$T(\boldsymbol{x}) = \overline{T}(\boldsymbol{x}), \qquad \boldsymbol{x} \in \Gamma_T$$

• Neumann b.c - prescribed flux on the boundary:

$$q_{\boldsymbol{n}}(\boldsymbol{x}) = \overline{q}_{\boldsymbol{n}}(\boldsymbol{x}), \qquad \boldsymbol{x} \in \Gamma_{qp},$$

where

$$q_{\boldsymbol{n}}(\boldsymbol{x}) = \left[\begin{array}{c} n_x(\boldsymbol{x}), n_y(\boldsymbol{x}) \end{array}\right] \left[\begin{array}{c} q_x(\boldsymbol{x}) \\ q_y(\boldsymbol{x}) \end{array}\right] = \boldsymbol{n}^{\mathrm{T}}(\boldsymbol{x})\boldsymbol{q}(\boldsymbol{x})$$

• Cauchy - Newton b.c. - heat transfer on the boundary:

$$q_{\boldsymbol{n}}(\boldsymbol{x}) = \alpha(\boldsymbol{x}) \left(T(\boldsymbol{x}) - T_{\infty}(\boldsymbol{x}) \right), \qquad \boldsymbol{x} \in \Gamma_{qc}$$

Non-linear b.c. (Newton) - heat radiation on the boundary:

$$q_{\boldsymbol{n}}(\boldsymbol{x}) = \varepsilon(\boldsymbol{x})\sigma(\boldsymbol{x})\left(T^{4}(\boldsymbol{x}) - T^{4}_{\infty}(\boldsymbol{x})\right), \qquad \boldsymbol{x} \in \Gamma_{qr}$$



Weighted residual method (Galerkin method):

• We are looking for a solution T(x) smooth enough, which fulfills $x \in \Omega$:

$$\boldsymbol{\nabla}^{\mathrm{T}} \left(\boldsymbol{\lambda}(\boldsymbol{x}) \boldsymbol{\nabla} T(\boldsymbol{x}) \right) + \overline{Q}(\boldsymbol{x}) = 0$$

• for $oldsymbol{x}\in\Gamma_T$: $T(oldsymbol{x})=\overline{T}(oldsymbol{x})$

• for $x \in \Gamma_q$:

$$-\boldsymbol{n}^{\mathrm{T}}(\boldsymbol{x})\boldsymbol{\lambda}(\boldsymbol{x})\boldsymbol{\nabla}T(\boldsymbol{x}) = \overline{q}_{\boldsymbol{n}}(\boldsymbol{x}),$$

where:

• for
$$\boldsymbol{x} \in \Gamma_{qp}$$
: $\overline{q}_{\boldsymbol{n}}(\boldsymbol{x})$ is prescribed
• for $\boldsymbol{x} \in \Gamma_{qc}$: $\overline{q}_{\boldsymbol{n}}(\boldsymbol{x}) = \alpha(\boldsymbol{x}) \left(T(\boldsymbol{x}) - T_{\infty}(\boldsymbol{x})\right)$
• for $\boldsymbol{x} \in \Gamma_{qr}$: $\overline{q}_{\boldsymbol{n}}(\boldsymbol{x}) = \varepsilon(\boldsymbol{x})\sigma(\boldsymbol{x}) \left(T^4(\boldsymbol{x}) - T_{\infty}^4(\boldsymbol{x})\right)$ (it is avoided in the derivation)



WEIGHTED RESIDUAL METHOD

Weighted residual method (Galerkin method):

For an arbitrary weight function δT so that $\delta T(\boldsymbol{x}) = 0$ for $\boldsymbol{x} \in \Gamma_T$, it holds:

$$\int_{\Omega} \delta T(\boldsymbol{x}) \left(\boldsymbol{\nabla}^{\mathrm{T}} \left(\boldsymbol{\lambda}(\boldsymbol{x}) \boldsymbol{\nabla} T(\boldsymbol{x}) \right) + \overline{Q}(\boldsymbol{x}) \right) \mathrm{d}\Omega = 0, \qquad \boldsymbol{x} \in \Omega$$

Integration by parts:

$$\int_{\Omega} g(\boldsymbol{x}) \frac{\partial f_x}{\partial x}(\boldsymbol{x}) \mathrm{d}\boldsymbol{x} = \int_{\Gamma} g(\boldsymbol{x}) n_x(\boldsymbol{x}) f_x(\boldsymbol{x}) \mathrm{d}\boldsymbol{s} - \int_{\Omega} \frac{\partial g}{\partial x}(\boldsymbol{x}) f_x(\boldsymbol{x}) \mathrm{d}\boldsymbol{x} \\ \int_{\Omega} g(\boldsymbol{x}) \frac{\partial f_y}{\partial y}(\boldsymbol{x}) \mathrm{d}\boldsymbol{x} = \int_{\Gamma} g(\boldsymbol{x}) n_y(\boldsymbol{x}) f_y(\boldsymbol{x}) \mathrm{d}\boldsymbol{s} - \int_{\Omega} \frac{\partial g}{\partial y}(\boldsymbol{x}) f_y(\boldsymbol{x}) \mathrm{d}\boldsymbol{x} \\ \int_{\Omega} g(\boldsymbol{x}) \boldsymbol{\nabla}^{\mathrm{T}} \boldsymbol{f}(\boldsymbol{x}) \mathrm{d}\boldsymbol{x} = \int_{\Gamma} g(\boldsymbol{x}) \boldsymbol{n}^{\mathrm{T}}(\boldsymbol{x}) \boldsymbol{f}(\boldsymbol{x}) \mathrm{d}\boldsymbol{s} - \int_{\Omega} (\boldsymbol{\nabla} g(\boldsymbol{x}))^{\mathrm{T}} \boldsymbol{f}(\boldsymbol{x}) \mathrm{d}\boldsymbol{x},$$

where

-

$$\boldsymbol{\nabla}^{\mathrm{T}} \boldsymbol{f}(\boldsymbol{x}) = \left[\begin{array}{c} \frac{\partial}{\partial x}, \frac{\partial}{\partial y} \end{array}
ight] \left[\begin{array}{c} f_x(\boldsymbol{x}) \\ f_y(\boldsymbol{x}) \end{array}
ight] = rac{\partial f_x}{\partial x}(\boldsymbol{x}) + rac{\partial f_y}{\partial y}(\boldsymbol{x})$$



Weighted residual method (Galerkin method):

• We apply the divergence theorem for $\delta T = g$ a $f = \lambda(x) \nabla T(x)$:

$$\int_{\Omega} \delta T(\boldsymbol{x}) \left(\boldsymbol{\nabla}^{\mathrm{T}} \left(\boldsymbol{\lambda}(\boldsymbol{x}) \boldsymbol{\nabla} T(\boldsymbol{x}) \right) + \overline{Q}(\boldsymbol{x}) \right) \mathrm{d}\Omega = \\ = \int_{\Gamma} \delta T(\boldsymbol{x}) \boldsymbol{n}^{\mathrm{T}}(\boldsymbol{x}) \boldsymbol{\lambda}(\boldsymbol{x}) \boldsymbol{\nabla} T(\boldsymbol{x}) \mathrm{d}\Gamma - \int_{\Omega} \left(\boldsymbol{\nabla} \delta T(\boldsymbol{x}) \right)^{\mathrm{T}} \boldsymbol{\lambda}(\boldsymbol{x}) \boldsymbol{\nabla} T(\boldsymbol{x}) (\boldsymbol{x}) \mathrm{d}\Omega + \int_{\Omega} \delta T(\boldsymbol{x}) \overline{Q}(\boldsymbol{x}) \mathrm{d}\Omega,$$

where the integral on the boundary can be split into two parts:

$$\int_{\Gamma} \delta T(\boldsymbol{x}) \boldsymbol{n}^{\mathrm{T}}(\boldsymbol{x}) \boldsymbol{\lambda}(\boldsymbol{x}) \boldsymbol{\nabla} T(\boldsymbol{x}) \mathrm{d}\Gamma = \int_{\Gamma_{T}} \widetilde{\delta T(\boldsymbol{x})} \boldsymbol{n}^{\mathrm{T}}(\boldsymbol{x}) \boldsymbol{\lambda}(\boldsymbol{x}) \boldsymbol{\nabla} T(\boldsymbol{x}) \mathrm{d}\Gamma + \int_{\Gamma_{q}} \delta T(\boldsymbol{x}) \underbrace{\boldsymbol{n}^{\mathrm{T}}(\boldsymbol{x}) \boldsymbol{\lambda}(\boldsymbol{x}) \boldsymbol{\nabla} T(\boldsymbol{x})}_{=-q \boldsymbol{n}} \mathrm{d}\Gamma$$



It follows:

$$\int_{\Gamma_q} \delta T(\boldsymbol{x}) q_{\boldsymbol{n}}(\boldsymbol{x}) \mathrm{d}\Gamma = \int_{\Gamma_{qp}} \delta T(\boldsymbol{x}) \overline{q}_{\boldsymbol{n}}(\boldsymbol{x}) \mathrm{d}\Gamma + \int_{\Gamma_{qc}} \delta T(\boldsymbol{x}) \alpha(\boldsymbol{x}) \left(T(\boldsymbol{x}) - T_{\infty}(\boldsymbol{x})\right) \mathrm{d}\Gamma$$

Weak form:

$$\begin{split} \int_{\Omega} \boldsymbol{\nabla}^{\mathrm{T}} \delta T(\boldsymbol{x}) \boldsymbol{\lambda}(\boldsymbol{x}) \boldsymbol{\nabla} T(\boldsymbol{x}) \mathrm{d}\Omega &+ \int_{\Gamma_{qc}} \delta T(\boldsymbol{x}) \alpha(\boldsymbol{x}) T(\boldsymbol{x}) \mathrm{d}\Gamma = \int_{\Gamma_{qp}} \delta T(\boldsymbol{x}) \overline{q}_{\boldsymbol{n}}(\boldsymbol{x}) \mathrm{d}\Gamma + \\ &+ \int_{\Gamma_{qc}} \delta T(\boldsymbol{x}) \alpha(\boldsymbol{x}) T_{\infty}(\boldsymbol{x}) \mathrm{d}\Gamma + \int_{\Omega} \delta T(\boldsymbol{x}) \overline{Q}(\boldsymbol{x}) \mathrm{d}\Omega \end{split}$$

We are looking for such an admissible trial solution T(x) which satisfies the above formulation.



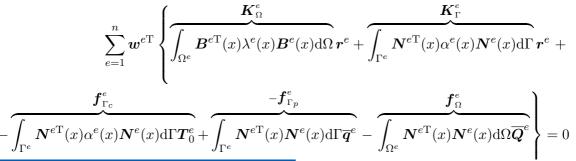
FINITE ELEMENT METHOD

Finite Element Method:

- \blacksquare The domain Ω is discretized by finite elements and nodes
- The weak form is expressed by an approximation of the trial solution and the weight function in elements. The approximation solution requires C^0 continuity
- \blacksquare The temperature function T is approximated in each element in the following shape:

$$T^{e}(\boldsymbol{x}) \approx \boldsymbol{N}^{e}(\boldsymbol{x})\boldsymbol{r}^{e}, \quad \boldsymbol{\nabla}T^{e}(\boldsymbol{x}) \approx \boldsymbol{B}^{e}(\boldsymbol{x})\boldsymbol{r}^{e}, \quad \delta T^{e}(\boldsymbol{x}) \approx \boldsymbol{N}^{e}(\boldsymbol{x})\boldsymbol{w}^{e}, \quad \boldsymbol{\nabla}\delta T^{e}(\boldsymbol{x}) \approx \boldsymbol{B}^{e}(\boldsymbol{x})\boldsymbol{w}^{e}$$

Introducing approximations of trial solution and weight function into the weak form (for all w^e that $w^e = 0$ on Γ_T), we obtain the following equation, where the integrals of the weak form are transferred into the sum of integrals in elements:





FINITE ELEMENT METHOD

Finite Element Method:

Global quantities - localization, for which is introduced the distribution function for an each element: L^e such that it is valid $r^e = L^e r$:

$$\boldsymbol{w}^{\mathrm{T}} \sum_{e=1}^{n} \left((\boldsymbol{L}^{e\mathrm{T}} \boldsymbol{K}_{\Omega}^{e} \boldsymbol{L}^{e} + \boldsymbol{L}^{e\mathrm{T}} \boldsymbol{K}_{\Gamma}^{e} \boldsymbol{L}^{e}) \boldsymbol{r} - \boldsymbol{L}^{e\mathrm{T}} \boldsymbol{f}_{\Gamma_{c}}^{e} - \boldsymbol{L}^{e\mathrm{T}} \boldsymbol{f}_{\Gamma_{p}}^{e} - \boldsymbol{L}^{e\mathrm{T}} \boldsymbol{f}_{\Omega}^{e} \right) = 0,$$

We can write:

$$\boldsymbol{w}^{\mathrm{T}}\left(\sum_{e=1}^{n} \hat{\boldsymbol{K}}^{e} \boldsymbol{r} - \sum_{e=1}^{n} \hat{\boldsymbol{f}}^{e}\right) = 0$$

Finaly, we have:

$$Kr = f$$

Decomposition of the conductivity matrix according to Dirichlet b.c. (r_d) :

$$\left[egin{array}{ccc} m{K}_{TT} & m{K}_{Td} \ m{K}_{dT} & m{K}_{dd} \end{array}
ight] \left[egin{array}{ccc} m{r}_T \ m{r}_d \end{array}
ight] = \left[egin{array}{ccc} m{f}_T \ m{f}_d \end{array}
ight] + \left[egin{array}{ccc} m{0} \ m{R} \end{array}
ight],$$

where

$$\boldsymbol{K}_{TT}\boldsymbol{r}_{T} = \boldsymbol{f}_{T} - \boldsymbol{K}_{Td}\boldsymbol{r}_{d}$$

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- English course of "Numerical analysis of structures" by J. Zeman (jan.zeman@fsv.cvut.cz)
- Czech course of "Numerická analýza konstrukcí" (Numerical analysis of structures) by B. Patzák (borek.patzak@fsv.cvut.cz)
- J. Fish and T. Belytschko: A First Course in Finite Elements, John Wiley & Sons, 2007

