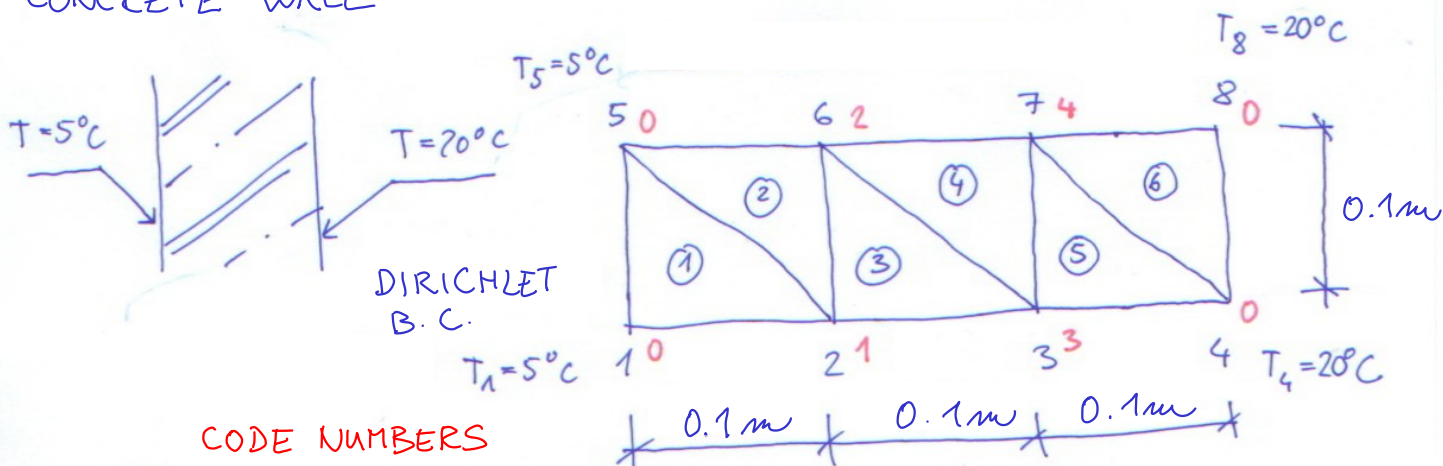


2D HEAT CONDUCTION PROBLEM

BENCHMARK NO. 1

$$\lambda = 2 \text{ W} \cdot \text{m}^{-1} \cdot \text{K}^{-1}$$

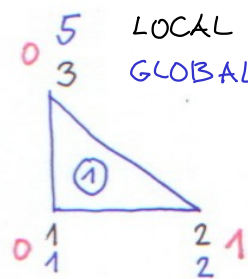
CONCRETE WALL



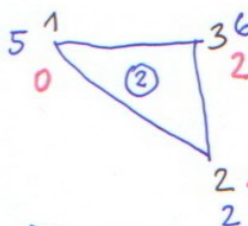
CODE NUMBERS

LOCAL NUMBERING

GLOBAL NUMBERING



$$B_1^e = \frac{1}{2A_1} \begin{bmatrix} -0,1 & 0,1 & 0 \\ -0,1 & 0 & 0,1 \end{bmatrix}$$



$$B_2^e = \frac{1}{2A_2} \begin{bmatrix} -0,1 & 0 & 0,1 \\ 0 & -0,1 & 0,1 \end{bmatrix}$$

$$B^e = \begin{bmatrix} \frac{\partial N_1}{\partial x} & \frac{\partial N_2}{\partial x} & \frac{\partial N_3}{\partial x} \\ \frac{\partial N_1}{\partial y} & \frac{\partial N_2}{\partial y} & \frac{\partial N_3}{\partial y} \end{bmatrix}$$

$$A_1 = A_2$$

$$K_1^e = \frac{\lambda}{4A_1} \begin{bmatrix} 0,02 & -0,01 & -0,01 \\ -0,01 & 0,01 & 0 \\ -0,01 & 0 & 0,01 \end{bmatrix} \begin{matrix} 0 & 1 & 3 \\ 1 & 3 & 0 \\ 0 & 2 & 4 \\ 0 & 1 & 0 \end{matrix}$$

$$K_2^e = \frac{\lambda}{4A_2} \begin{bmatrix} 0,01 & 0 & -0,01 \\ 0 & 0,01 & -0,01 \\ -0,01 & -0,01 & 0,02 \end{bmatrix} \begin{matrix} 0 & 2 & 4 \\ 1 & 3 & 0 \\ 2 & 4 & 0 \\ 0 & 1 & 2 \end{matrix}$$

$$B^e = \frac{1}{2A} \begin{bmatrix} y_{23} & y_{31} & y_{12} \\ x_{32} & x_{13} & x_{21} \end{bmatrix}$$

$$K^e = A B^{eT} \lambda B^e$$

ELEMENT ①

$$K_1^e = \frac{\lambda}{4A_1} \begin{bmatrix} -0,1 & -0,1 \\ 0,1 & 0 \\ 0 & 0,1 \end{bmatrix} \begin{bmatrix} -0,1 & 0,1 & 0 \\ -0,1 & 0 & 0,1 \end{bmatrix}$$

LOCALIZATION \Rightarrow

ELEMENTS: 1 3 5
2 4 6

GLOBAL CONDUCTIVITY MATRIX:
- SYMMETRIC

RIGHT-HAND SIDE VECTOR:

$$K = \frac{\lambda}{4A} \begin{bmatrix} 0,04 & -0,02 & -0,01 & 0 \\ & 0,04 & 0 & -0,01 \\ & & 0,04 & -0,02 \\ & & & 0,04 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \end{matrix}$$

$$f = \begin{Bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

$$\underline{K} \underline{r} = \underline{f} - \underline{d}$$

$\underline{d} = \underline{K}_d \underline{r}_d$ = CONTRIBUTION FROM DIRICHLET B.C.
- PRESCRIBED TEMPERATURES

$$d = \frac{\lambda}{4A} \begin{Bmatrix} -0,05 \\ -0,05 \\ -0,2 \\ -0,2 \end{Bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \end{matrix}$$

ELEMENT ①

$$\frac{\lambda}{4A} \begin{bmatrix} 0,02 & -0,01 & -0,01 \\ -0,01 & 0,01 & 0 \\ -0,01 & 0 & 0,01 \end{bmatrix} \begin{Bmatrix} 5 \\ 0 \\ 5 \end{Bmatrix} \begin{matrix} 0 \\ 1 \\ 0 \end{matrix} = \begin{Bmatrix} 0,05 \\ -0,05 \\ 0 \end{Bmatrix} \begin{matrix} 0 \\ 1 \\ 0 \end{matrix}$$

ELEMENT ②

$$\frac{\lambda}{4A} \begin{bmatrix} 0,01 & 0 & -0,01 \\ 0 & 0,01 & -0,01 \\ -0,01 & -0,01 & 0,02 \end{bmatrix} \begin{Bmatrix} 5 \\ 0 \\ 0 \end{Bmatrix} \begin{matrix} 0 \\ 1 \\ 2 \end{matrix} = \begin{Bmatrix} 0,05 \\ 0 \\ -0,05 \end{Bmatrix} \begin{matrix} 0 \\ 1 \\ 2 \end{matrix}$$

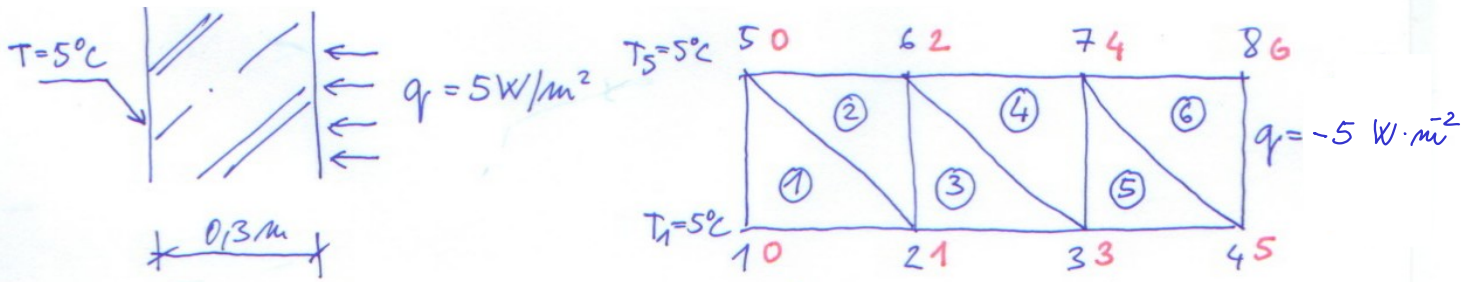
PROBLEM SOLUTION:

$$r = \begin{Bmatrix} T_2 \\ T_6 \\ T_3 \\ T_7 \end{Bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \end{matrix} = \begin{Bmatrix} 10 \\ 10 \\ 15 \\ 15 \end{Bmatrix}$$

THE SAME PRINCIPLE OF LOCALIZATION FOR ELEMENTS ⑤ AND ⑥

$$\frac{\lambda}{4 \cdot A} = \frac{2}{4 \cdot 0,1 \cdot 0,1/2} = 100$$

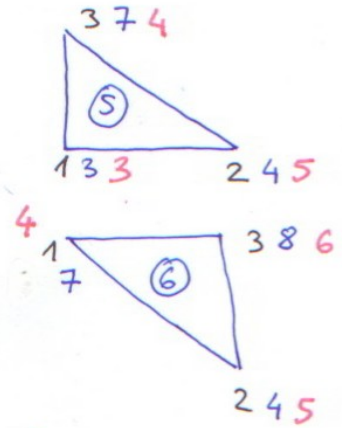
BENCHMARK NO. 2



CONDUCTIVITY MATRIX OF THE PROBLEM

- WE USE COND. MATRIX FROM PREVIOUS EXAMPLE, AND EXPAND IT BY COMPONENTS IN POSITIONS 3 TO 6

$$K = \frac{\lambda}{4A} \begin{bmatrix} 0,04 & -0,02 & -0,01 & 0 & 0 & 0 \\ 0,04 & 0 & -0,01 & 0 & 0 & 0 \\ & 0,04 & -0,02 & -0,01 & 0 & 0 \\ & & 0,04 & 0 & -0,01 & 0 \\ & & & 0,02 & -0,01 & 0 \\ & & & & 0,02 & 0 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{matrix}$$



$$K_5^e = \frac{\lambda}{4A} \begin{bmatrix} 0,02 & -0,01 & -0,01 \\ -0,01 & 0,01 & 0 \\ -0,01 & 0 & 0,01 \end{bmatrix} \begin{matrix} 3 \\ 4 \\ 5 \end{matrix}$$

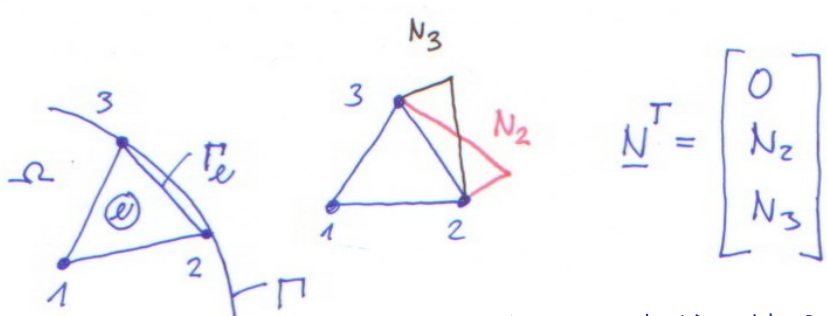
RIGHT-HAND SIDE:

$K_d \cdot r_d = d$ = CONTRIBUTION FROM DIRICHLET B.C. IN ELEMENTS NO. ① AND ②

$$K_6^e = \frac{\lambda}{4A} \begin{bmatrix} 0,01 & 0 & -0,01 \\ 0 & 0,01 & -0,01 \\ -0,01 & -0,01 & 0,02 \end{bmatrix} \begin{matrix} 4 \\ 5 \\ 6 \end{matrix}$$

$$d = \begin{Bmatrix} -0,05 \\ -0,05 \\ 0 \\ 0 \\ 0 \\ 0 \end{Bmatrix}$$

LOADING VECTOR FROM PRESCRIBED FLUX:



LINEAR APPROXIMATION ON THE EDGE !!

LOADING VECTOR FROM PRESCRIBED FLUX:

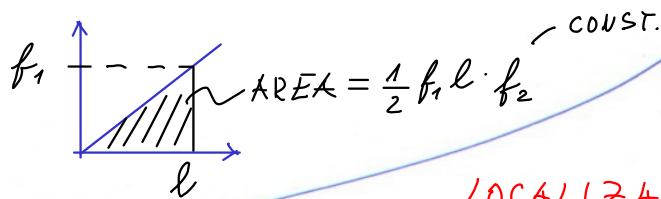
\bar{q} IS NEGATIVE AND CONSTANT

$$f = - \int_{\Gamma_{qp}} \underbrace{N^e}_N \bar{q} d\Gamma = \int_{\Gamma_{qp}} -N^e \bar{q} d\Gamma$$

$$f_G^e = - \int_l \begin{bmatrix} 0 \\ N_2 \\ N_3 \end{bmatrix} [-5] d\Gamma = \frac{1}{2} l \begin{bmatrix} 0 \\ 5 \\ 5 \end{bmatrix} = \begin{bmatrix} 0 \\ 0,25 \\ 0,25 \end{bmatrix}$$

NOTE: INTEGRAL OF MULTIPLICATION OF LINEAR AND CONSTANT FUNCTION:

$$\int_l \triangle \square dx = \frac{1}{2} f_1 f_2 l$$



$$f = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 0,25 \\ 0,25 \end{bmatrix}$$

LOCALIZATION

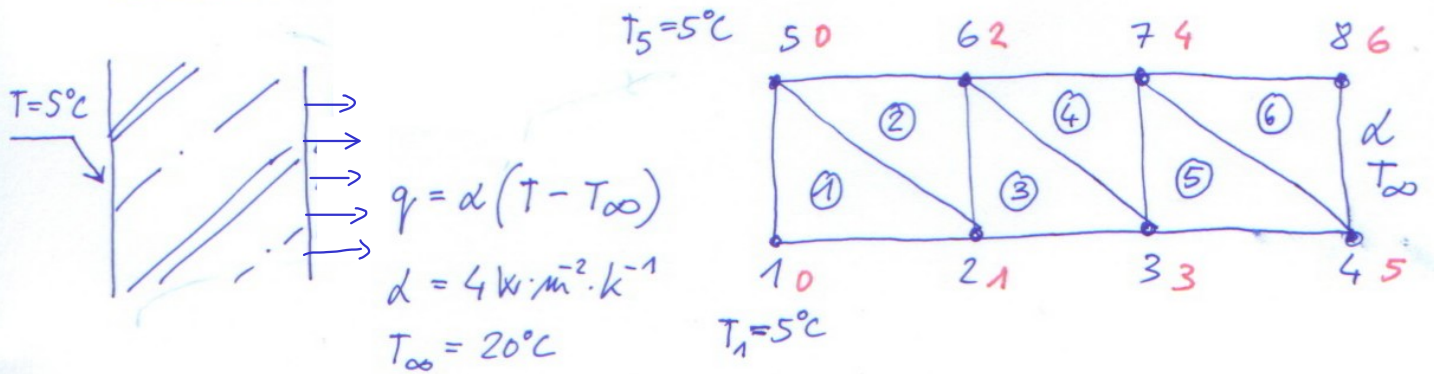
PROBLEM SOLUTION:

$$K r = f - d$$

$$r = \begin{bmatrix} T_2 \\ T_6 \\ T_3 \\ T_7 \\ T_4 \\ T_8 \end{bmatrix} = \begin{bmatrix} 5,25 \\ 5,25 \\ 5,5 \\ 5,5 \\ 5,75 \\ 5,75 \end{bmatrix}$$

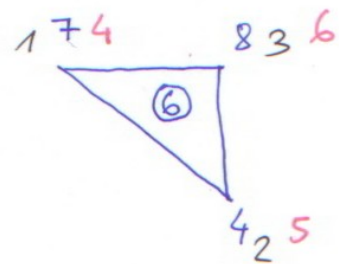
BENCHMARK NO. 3

DISCRETIZATION:



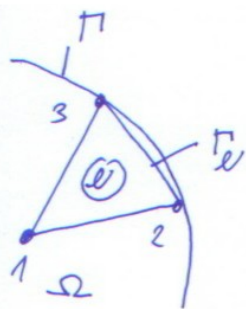
WE USE THE COND. MATRIX FROM PREVIOUS BENCHMARK:

$$K = \frac{\lambda}{4A} \begin{bmatrix} 0,04 & -0,02 & -0,01 & 0 & 0 & 0 \\ -0,02 & 0,04 & 0 & -0,01 & 0 & 0 \\ & & 0,04 & -0,02 & -0,01 & 0 \\ & & & 0,04 & 0 & -0,01 \\ & & & & 0,02 & -0,01 \\ & & & & & 0,02 \end{bmatrix}$$



THE CONTRIBUTION FROM THE HEAT TRANSMISSION B.C. IS LOCALIZED IN THIS PART. BEFORE THAT, THE MATRIX IS MULTIPLIED BY $\frac{\lambda}{4 \cdot A} = 100$

BOUNDARY CONDITION:



$$\underline{N} = [0, N_2, N_3]$$

$$K_{\Gamma,6}^e = \int_{\Gamma_{qc}^e} \underline{N}^e \alpha \underline{N}^e d\Gamma = \int_l \begin{bmatrix} 0 \\ N_2 \\ N_3 \end{bmatrix} \alpha [0, N_2, N_3] d\Gamma$$

$$= \alpha \int_l \begin{bmatrix} 0 & 0 & 0 \\ 0 & N_2 N_2 & N_2 N_3 \\ 0 & N_3 N_2 & N_3 N_3 \end{bmatrix} d\Gamma = \alpha l \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1/3 & 1/6 \\ 0 & 1/6 & 1/3 \end{bmatrix}$$

INTEGRAL OF TWO LINEAR FUNCTION MULTIPLICATION:

$$\int_l \begin{matrix} f_1 \\ \triangle \\ f_2 \end{matrix} dx = \frac{1}{3} f_1 f_2 l \quad ; \quad \int_l \begin{matrix} f_1 \\ \triangle \\ f_2 \end{matrix} dx = \frac{1}{6} f_1 f_2 l$$

$$\underline{k}_{\Gamma,6}^e = 4 \cdot 0,1 \begin{bmatrix} 0 & 0 & 0 \\ 0 & 1/3 & 1/6 \\ 0 & 1/6 & 1/3 \end{bmatrix} \begin{matrix} 4 \\ 5 \\ 6 \end{matrix} \Rightarrow \text{LOCALIZATION}$$

CONTRIBUTION TO THE RIGHT-HAND SIDE:

CONSTANT PARAMETERS

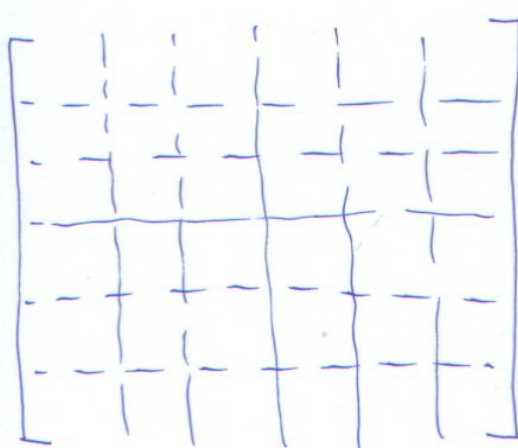
$$\underline{f}_{\Gamma,6}^e = \int_{\Gamma_{qc}^e} \underline{N}^{eT} \alpha(x) T_{\infty}(x) d\Gamma = \int_l \underline{N}^{eT} \alpha T_{\infty} d\Gamma =$$

$$= \int_l \begin{bmatrix} 0 \\ N_2 \\ N_3 \end{bmatrix} 4 \cdot 20 d\Gamma = 4 \cdot 20 \cdot \frac{1}{2} l \begin{bmatrix} 0 \\ 1 \\ 1 \end{bmatrix} = \begin{bmatrix} 0 \\ 4 \\ 4 \end{bmatrix} \begin{matrix} 4 \\ 5 \\ 6 \end{matrix} \Rightarrow$$

LOCALIZATION

RESULTING SYSTEM OF EQUATION:

FROM THE PREV. BENCHMARK

$$\underline{K} \cdot \underline{r} = \underline{f} - \underline{d}$$


$$\begin{bmatrix} T_2 \\ T_6 \\ T_3 \\ T_7 \\ T_4 \\ T_8 \end{bmatrix} \begin{matrix} 1 \\ 2 \\ 3 \\ 4 \\ 5 \\ 6 \end{matrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \\ 4 \\ 4 \end{bmatrix} - \begin{bmatrix} -0,05 \\ -0,05 \\ 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\underline{r} = \begin{bmatrix} 6,875 \\ 6,875 \\ 8,75 \\ 8,75 \\ 10,625 \\ 10,625 \end{bmatrix}$$

SOLUTION