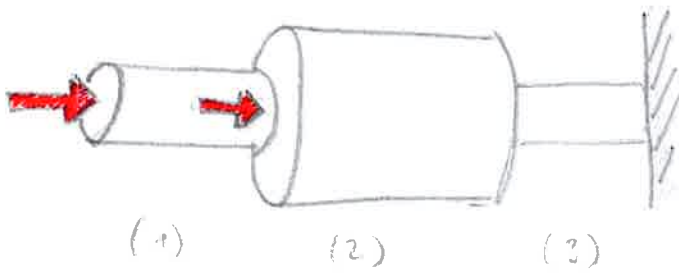


HANDOUT 1

Finite Element Method (FEM):

- ① SUBDIVISION of a problem into finite elements



trusses ⊕ nodes whenever loads are applied

⊕ nodes where section / material properties change

- ② ELEMENT FORMULATION

response of the structure to loading ⇒ stiffness matrix

- ③ ASSEMBLY

putting all element equations together to get global equations of the entire system

- ④ SOLUTION

- ⑤ POST-PROCESSING

stresses, strains, visualization, ...

BAR ELEMENT

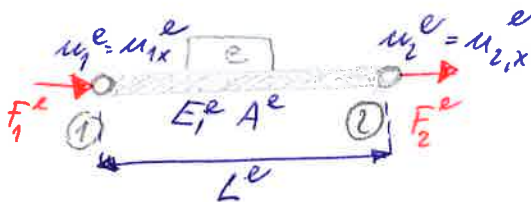
- slender (very thin) and straight

→ negligible resistance to

→ only axial internal forces
(similar to springs)

torsion
shear
bending

- notation



superscript... element number
superscript... mode number

GOVERNING EQUATIONS

1) EQUILIBRIUM : $F_1^e + F_2^e = 0$

2) STRESS-STRAIN (HOOKE'S) LAW : $\sigma^e = E^e \cdot \epsilon^e$

- linear & elasticity
- ϵ - strain
- σ - stress

3) COMPATIBILITY : $\epsilon^e = \frac{\delta^e}{L^e} = \frac{u_2^e - u_1^e}{L^e}$

- no gaps, overlaps
- continuous structure

internal axial force

$F_2^e = F^e = A^e \cdot \sigma^e = A^e \cdot E^e \cdot \epsilon^e = A^e E^e \cdot \frac{u_2^e - u_1^e}{L^e} = -A^e E^e \frac{u_1^e - u_2^e}{L^e}$

$F_1^e = -F^e = A^e E^e \frac{u_1^e - u_2^e}{L^e}$

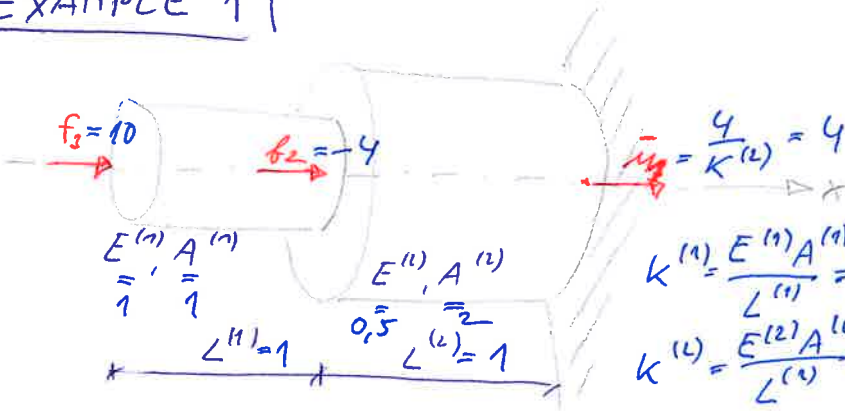
in matrix form:

$$\begin{bmatrix} F_1^e \\ F_2^e \end{bmatrix} = \frac{A^e E^e}{L^e} \begin{bmatrix} 1 & -1 \\ -1 & 1 \end{bmatrix} \begin{bmatrix} u_1^e \\ u_2^e \end{bmatrix}$$

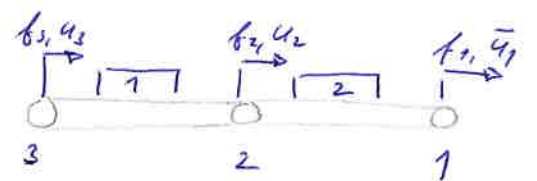
$\underline{F}^e = \underline{K}^e \underline{d}^e$

symmetric stiffness matrix

EXAMPLE 1

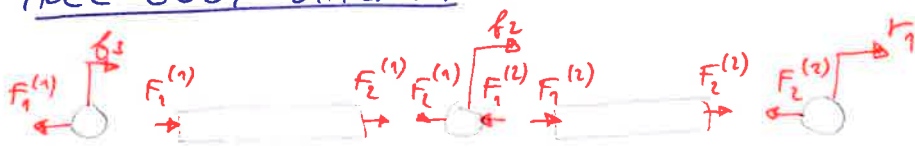


SCHEME



- 1) SUBDIVISION - forces, mat. properties
- 2) NUMBERING
- 3) UNKNOWN - EITHER force or displacement + relation through stiffness matrix

FREE-BODY DIAGRAM



4) ELEMENT STIFFNESS EQUATIONS OF ALL BARS
 → relate nodal forces to nodal displacements

5) ASSEMBLY

EQUILIBRIUM OF NODES

$$\begin{matrix} \textcircled{1} \\ \textcircled{2} \\ \textcircled{3} \end{matrix} \begin{bmatrix} 0 \\ F_2^{(1)} \\ F_1^{(1)} \end{bmatrix} + \begin{bmatrix} F_2^{(2)} \\ F_1^{(2)} \\ 0 \end{bmatrix} = \begin{bmatrix} r_1 \\ -4 \\ f_3^{10} \end{bmatrix} = \begin{bmatrix} 0 \\ -4 \\ f_3^{10} \end{bmatrix} + \begin{bmatrix} r_1 \\ 0 \\ 0 \end{bmatrix}$$

PRESCRIBED UNKNOWN REACTIONS

$$\begin{bmatrix} 0 & 0 & 0 \\ 0 & k^{(1)} & -k^{(1)} \\ 0 & -k^{(1)} & k^{(1)} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} + \begin{bmatrix} k^{(2)} & -k^{(2)} & 0 \\ -k^{(2)} & k^{(2)} & 0 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} 0 \\ f_2 \\ f_3 \end{bmatrix} + \begin{bmatrix} r_1 \\ 0 \\ 0 \end{bmatrix}$$

$\underline{K}^{(1)} \underline{d} + \underline{K}^{(2)} \underline{d} = \underline{F} + \underline{r}$
 $\underline{K} = \sum_{e=1}^{ne} \underline{K}^e \qquad \underline{K} \cdot \underline{d} = \underline{F} + \underline{r}$

E-modes

→ "essential", known displacements

F-modes

→ "free", unknown displacements

$$\underline{d} = \begin{bmatrix} \bar{d}_E \\ d_F \end{bmatrix} \qquad \underline{F} = \begin{bmatrix} \bar{F}_E \\ \underline{F}_F \end{bmatrix} \qquad \underline{r} = \begin{bmatrix} \bar{r}_E \\ \underline{r}_F \end{bmatrix}$$

$$\begin{bmatrix} k^{(2)} & -k^{(2)} & 0 \\ -k^{(2)} & k^{(1)}+k^{(2)} & -k^{(1)} \\ 0 & -k^{(1)} & k^{(1)} \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} r_1 \\ f_2 \\ f_3 \end{bmatrix} \iff \begin{bmatrix} \underline{K}_E & \underline{K}_{EF} \\ \underline{K}_{EF}^T & \underline{K}_F \end{bmatrix} \begin{bmatrix} \bar{d}_E \\ d_F \end{bmatrix} = \begin{bmatrix} \bar{r}_E \\ \underline{r}_F \end{bmatrix}$$

$$\underline{K}_{EF}^T \bar{d}_E + \underline{K}_F d_F = \underline{r}_F \implies d_F = \underline{K}_F^{-1} (\underline{r}_F - \underline{K}_{EF}^T \bar{d}_E)$$

$$\underline{r}_E = \underline{K}_E \bar{d}_E + \underline{K}_{EF} d_F$$

$$\delta_{\underline{F}} = \begin{bmatrix} u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} k^{(1)} + k^{(2)} & -k^{(1)} \\ -k^{(1)} & k^{(1)} \end{bmatrix}^{-1} \left\{ \begin{bmatrix} -4 \\ 10 \end{bmatrix} - \begin{bmatrix} -k^{(2)} \\ 0 \end{bmatrix} \left[\frac{4}{k^{(2)}} \right] \right\}$$

$$u_2 = \frac{10}{k^{(1)}} \quad u_3 = 10 \left(\frac{1}{k^{(1)}} + \frac{1}{k^{(2)}} \right)$$

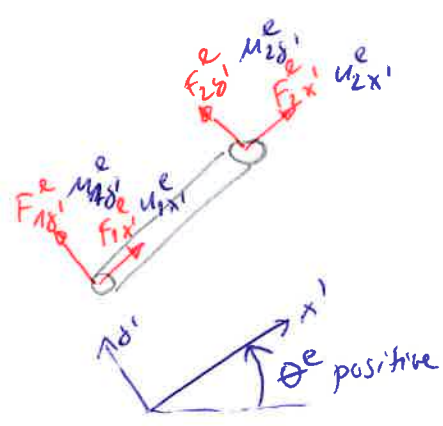
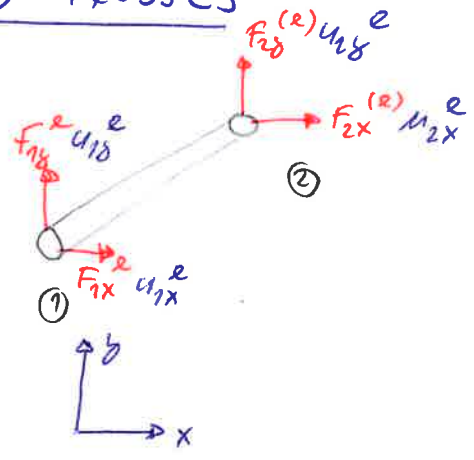
$$r_1 = k^{(2)} \cdot \frac{4}{k^{(2)}} + \begin{bmatrix} -k^{(2)} & 0 \end{bmatrix} \cdot \begin{bmatrix} \frac{10}{k^{(1)}} \\ 10 \cdot \left(\frac{1}{k^{(1)}} + \frac{1}{k^{(2)}} \right) \end{bmatrix} = -6$$

OR:

$$\begin{bmatrix} k^{(1)} + k^{(2)} & -k^{(1)} \\ -k^{(1)} & k^{(1)} \end{bmatrix} \begin{bmatrix} u_2 \\ u_3 \end{bmatrix} = \begin{bmatrix} -4 \\ 10 \end{bmatrix} - \begin{bmatrix} -k^{(2)} \\ 0 \end{bmatrix} \left[\frac{4}{k^{(2)}} \right]$$

STRAINS, STRESSES
 $\epsilon^{(1)} = -10$ $\sigma^{(1)} = -10$
 $\epsilon^{(2)} = -6$ $\sigma^{(2)} = -3$ } compression
 $\Rightarrow u_2 = 10$
 $u_3 = 20$

2D TRUSSES



$$\underline{F}^e = \begin{bmatrix} F_{1x}^e \\ F_{1y}^e \\ F_{2x}^e \\ F_{2y}^e \end{bmatrix} \quad \underline{d}^e = \begin{bmatrix} d_{1x}^e \\ d_{1y}^e \\ d_{2x}^e \\ d_{2y}^e \end{bmatrix}$$

2 unknowns per node

a) COORDINATE TRANSFORMATIONS

$$c^e = \cos \theta^e \quad s^e = \sin \theta^e$$

$$\left. \begin{aligned} u_{1x'}^e &= u_{1x}^e \cdot \cos \theta^e + u_{1y}^e \cdot \sin \theta^e \\ u_{1y'}^e &= -u_{1x}^e \cdot \sin \theta^e + u_{1y}^e \cdot \cos \theta^e \\ u_{2x'}^e &= \dots \\ u_{2y'}^e &= \dots \end{aligned} \right\} \begin{bmatrix} u_{1x'}^e \\ u_{1y'}^e \\ u_{2x'}^e \\ u_{2y'}^e \end{bmatrix} = \begin{bmatrix} c^e & s^e & 0 & 0 \\ -s^e & c^e & 0 & 0 \\ 0 & 0 & c^e & s^e \\ 0 & 0 & -s^e & c^e \end{bmatrix} \begin{bmatrix} u_{1x}^e \\ u_{1y}^e \\ u_{2x}^e \\ u_{2y}^e \end{bmatrix}$$

$$c^e = \frac{x_2^e - x_1^e}{L^e}$$

$$s^e = \frac{y_2^e - y_1^e}{L^e}$$

T^e - rotation matrix
 orthogonal $(T^e)^{-1} = (T^e)^T$
 $T^e (T^e)^T = I$

b) Expanded 1D stiffness equation

$$\begin{bmatrix} k^e & -k^e \\ -k^e & k^e \end{bmatrix} \begin{bmatrix} u_{1x1}^e \\ u_{2x1}^e \end{bmatrix} = \begin{bmatrix} F_{1x1}^e \\ F_{2x1}^e \end{bmatrix}$$

$$\underbrace{K^{ie}}_{\underline{K}^{ie}} \begin{bmatrix} 1 & 0 & -1 & 0 \\ 0 & 0 & 0 & 0 \\ -1 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \underbrace{d^{ie}}_{\underline{d}^{ie}} = \underbrace{\begin{bmatrix} F_{1x1}^e \\ F_{1y1}^e \\ F_{2x1}^e \\ F_{2y1}^e \end{bmatrix}}_{\underline{F}^{ie}} \left. \begin{matrix} \rightarrow 0 \\ \rightarrow 0 \end{matrix} \right\} \text{shear forces negligible}$$

$$\underline{K}^{ie} \cdot \underline{d}^{ie} = \underline{F}^{ie}$$

$$\underline{K}^{ie} \cdot \underline{T}^e \cdot \underline{d}^e = \underline{T}^e \cdot \underline{F}^e \quad / \cdot (\underline{T}^e)^{-1}$$

$$(\underline{T}^e)^{-1} \underline{K}^{ie} \underline{T}^e \underline{d}^e = \underline{T}^e \underline{F}^e \quad / (\underline{T}^e)^{-1} = (\underline{T}^e)^T$$

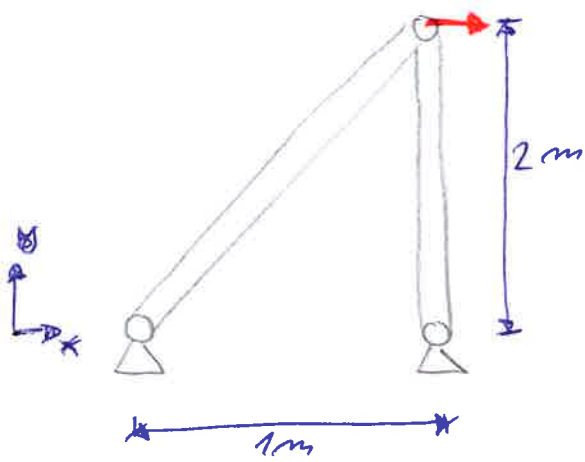
$$\underbrace{(\underline{T}^e)^T \underline{K}^{ie} \underline{T}^e}_{\underline{K}^e} \underline{d}^e = \underline{F}^e$$

$$\underline{K}^e = (\underline{T}^e)^T \underline{K}^{ie} \underline{T}^e = \begin{bmatrix} c^e & -s^e & 0 & 0 \\ s^e & c^e & 0 & 0 \\ 0 & 0 & c^e & -s^e \\ 0 & 0 & s^e & c^e \end{bmatrix} \frac{E^e A^e}{L^e} \begin{bmatrix} c^e & s^e & 0 & 0 \\ -s^e & c^e & 0 & 0 \\ 0 & 0 & c^e & s^e \\ 0 & 0 & -s^e & c^e \end{bmatrix}^T$$

$$= \frac{E^e A^e}{L^e} \underbrace{\begin{bmatrix} c_e^2 & c_e s_e & -c_e^2 & -c_e s_e \\ c_e s_e & s_e^2 & -c_e s_e & -s_e^2 \\ -c_e^2 & -c_e s_e & c_e^2 & c_e s_e \\ -c_e s_e & -s_e^2 & c_e s_e & s_e^2 \end{bmatrix}}_{\underline{K}^e}$$

EXAMPLE 2

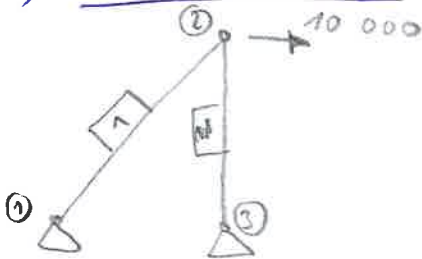
10 kN = 10 000 N



$$E = 200 \text{ GPa} = 200 \cdot 10^9 \text{ Pa} = 2 \cdot 10^{11} \text{ Pa}$$

$$A = 500 \text{ mm}^2 = 500 \cdot 10^{-6} \text{ m}^2 = 5 \cdot 10^{-4} \text{ m}^2$$

a) DISCRETIZATION



b) ELEMENT BEHAVIOR (LOCAL STIFFNESS MATRICES)

1) ①-②

$$\left. \begin{aligned} x_1^{(1)} &= 0 \text{ m} \\ x_2^{(1)} &= 1 \text{ m} \\ b_1^{(1)} &= 0 \text{ m} \\ b_2^{(1)} &= 2 \text{ m} \end{aligned} \right\}$$

$$L^{(1)} = \sqrt{(x_2^{(1)} - x_1^{(1)})^2 + (b_2^{(1)} - b_1^{(1)})^2} = \sqrt{1^2 + 2^2} = 2,236 \text{ m}$$

$$c^{(1)} = \frac{x_2^{(1)} - x_1^{(1)}}{L_1^{(1)}} = \frac{1}{2,236} = 0,447$$

$$s^{(1)} = \frac{b_2^{(1)} - b_1^{(1)}}{L_1^{(1)}} = \frac{2}{2,236} = 0,894$$

$$\underline{K}^{(1)} = \frac{200 \cdot 10^9 \cdot 500 \cdot 10^{-6}}{2,236} \cdot \begin{bmatrix} c^2 & cs & -c^2 & -cs \\ cs & s^2 & -cs & -s^2 \\ -c^2 & -cs & c^2 & cs \\ -cs & -s^2 & cs & s^2 \end{bmatrix} =$$

$$= 0,894 \cdot 10^6 \cdot \begin{bmatrix} 1 & 2 & -1 & -2 \\ 2 & 4 & -2 & -4 \\ -1 & -2 & 1 & 2 \\ -2 & -4 & 2 & 4 \end{bmatrix}$$

[N/m]

2) ② - ③

$$\left. \begin{aligned} x_1^{(2)} &= 1 \text{ m} \\ x_2^{(2)} &= 1 \text{ m} \\ \delta_1^{(2)} &= 2 \text{ m} \\ \delta_2^{(2)} &= 0 \text{ m} \end{aligned} \right\} \begin{aligned} L^{(2)} &= 2 \text{ m} \\ e^{(2)} &= 0 \\ \nu^{(2)} &= -1 \end{aligned}$$

$$K^{(2)} = 5 \cdot 10^7$$

$$\begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & -1 \\ 0 & 0 & 0 & 0 \\ 0 & -1 & 0 & 1 \end{bmatrix} \text{ [N/m]}$$

c) ASSEMBLY

$$\underline{K} = \begin{bmatrix} 0,894 & 1,788 & -0,894 & -1,788 & 0 & 0 \\ 1,788 & 3,576 & -1,788 & -3,576 & 0 & 0 \\ -0,894 & -1,788 & 0,894 & 1,788 & 0 & 0 \\ -1,788 & -3,576 & 1,788 & 8,576 & 0 & -5 \\ 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -5 & 0 & 5 \end{bmatrix} \cdot 10^7$$

① ② ③

$$\underline{d} = \begin{bmatrix} 0 \\ 0 \\ u_{2x} \\ u_{2y} \\ 0 \\ 0 \end{bmatrix} \quad \underline{F} = \begin{bmatrix} 0 \\ 0 \\ 10\,000 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

→ free DOFs 3 and 4

$$\underline{K}_F = 10^7 \cdot \begin{bmatrix} 0,894 & 1,788 \\ 1,788 & 8,576 \end{bmatrix}$$

$$\underline{d}_F = \begin{bmatrix} u_{2x} \\ u_{2y} \end{bmatrix}$$

$$\underline{F}_F = \begin{bmatrix} 10\,000 \\ 0 \end{bmatrix}$$

$$\underline{K}_E = 10^7 \cdot \begin{bmatrix} 0,894 & 1,788 & 0 & 0 \\ 1,788 & 3,576 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 5 \end{bmatrix}$$

$$\underline{d}_E = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 0 \end{bmatrix}$$

$$\underline{r}_E = \begin{bmatrix} r_{1x} \\ r_{1y} \\ r_{2x} \\ r_{2y} \end{bmatrix}$$

N

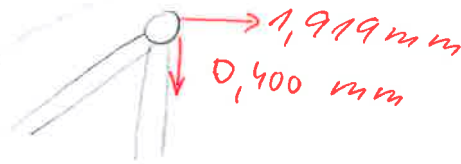
$$\underline{K}_{EF} = \begin{bmatrix} -0,894 & -1,788 \\ -1,788 & -3,576 \\ 0 & 0 \\ 0 & -5 \end{bmatrix} \cdot 10^7 \frac{N}{m}$$

⑧

D) SOLUTION

$$\underline{K}_F \underline{d}_F = \underline{f}_F - \underline{K}_{EF}^T \underline{d}_E = 0$$

$$10^7 \cdot \begin{bmatrix} 0,894 & 1,788 \\ 1,788 & 3,576 \end{bmatrix} \cdot \begin{bmatrix} u_{2x} \\ u_{2y} \end{bmatrix} = \begin{bmatrix} 10\,000 \\ 0 \end{bmatrix}$$



$$u_{2x} = 0,001\,919\,m$$

$$u_{2y} = -0,000\,4\,m$$

~~POST-PROCESSING~~

$$\underline{r}_E = \underline{K}_E \underline{d}_E + \underline{K}_{EF} \underline{d}_F = \begin{bmatrix} -0,894 & -1,788 \\ -1,788 & -3,576 \\ 0 & 0 \\ 0 & -5 \end{bmatrix} \cdot \begin{bmatrix} 0,001\,919 \\ -0,000\,4 \end{bmatrix} = \begin{bmatrix} -10\,000,00 \\ -20\,000,00 \\ 0 \\ 20\,000 \end{bmatrix}$$

$$\sum F_x = 0$$

$$\sum F_y = 0$$



E) POST-PROCESSING

$$\sigma^e = E^e \cdot \epsilon^e = E^e \cdot \frac{u_{2x}^e - u_{1x}^e}{L^e} = \frac{E^e}{L^e} \cdot [-1 \ 0 \ 1 \ 0] \cdot \begin{bmatrix} u_{1x}^e \\ u_{1y}^e \\ u_{2x}^e \\ u_{2y}^e \end{bmatrix} =$$

$$= \frac{E^e}{L^e} \cdot [-1 \ 0 \ 1 \ 0] \underline{T}^e \underline{d}^e = \frac{E^e}{L^e} [-c^e \ -s^e \ c^e \ s^e] \underline{d}^e$$

$$\sigma^{(1)} = \frac{200 \cdot 10^9}{2,236} \cdot \begin{bmatrix} -0,447 & -0,894 & 0,447 & 0,894 \end{bmatrix} \cdot \begin{bmatrix} 0 \\ 0 \\ 0,001\,919 \\ -0,000\,4 \end{bmatrix} =$$

$$= 44,76 \cdot 10^6 \text{ Pa}$$

$$\sigma^{(2)} = \frac{200 \cdot 10^9}{2} \cdot [0 \ 1 \ 0 \ -1] \cdot \begin{bmatrix} 0,001\,919 \\ -0,000\,4 \\ 0 \\ 0 \end{bmatrix} = -35,78 \cdot 10^6 \text{ Pa}$$